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Heart Rate Detection with Hilbert Vibration Decomposition Algorithm in Large-Scale Random Body Movements Based on FMCW Radars

Pei-Ling Cheng* and Chin-Lung Yang

Wireless Innovative System EM-Applied (WISE) Lab, Dep. of Electrical Engineering, National Cheng Kung University (NCKU), Tainan, Taiwan











Outline



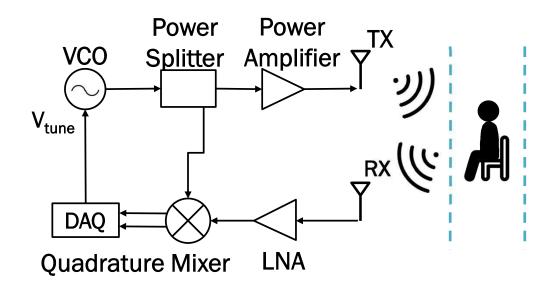
- Introduction and Motivation
- Literature Review
- Theory Analysis
- Proposed Method
- Measurement Results
- Conclusion





Introduction (1/2)





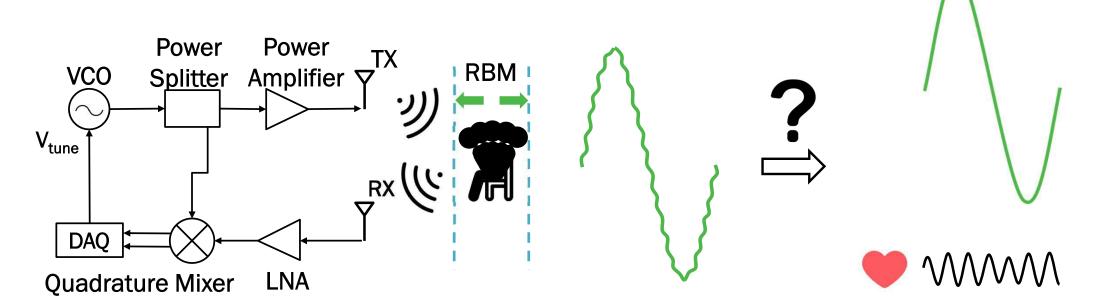






Introduction (2/2)









Motivation (1/2)



Motivation

- The environments are non-stationary in most of application scenarios
- Non-stationary clutter is aperiodic and uncertain
- The presence of RBM can seriously interfere with the extraction of vital signs
- Heart rate is difficult to identify compared with respiration

Goal

Heart rate detection in large-scale RBM based on FMCW radars

RBM: random body movement, FMCW: frequency modulated continuous wave







Motivation (2/2)



Problem solution

- FMCW radar system → Suitable SNR, Range resolution
- Hilbert Vibration Decomposition (HVD) → Cancellation RBM
- Masking signal HVD (M-HVD)→ Enhancing SNR

Challenge

- Accuracy of heartbeat extraction
- Reduce non-vital signs interference
- The SNR of heartbeat (quantify the effect of noise on heartbeat estimation)

SNR: signal-to-noise ratio





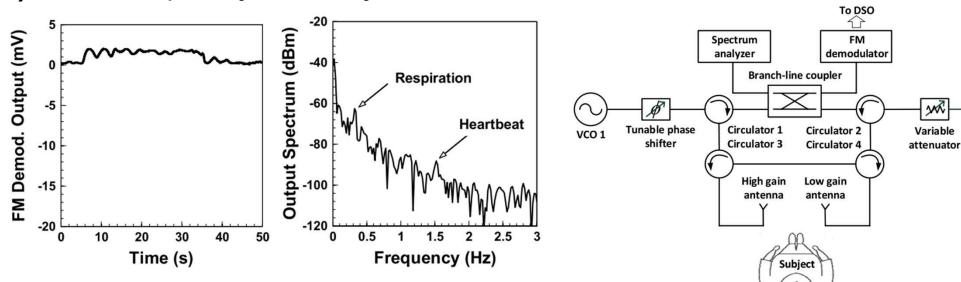


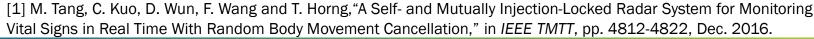
Literature Review (1/3)



VCO₂

- Self- and Mutually Injection-Locked (SMIL) [1]
 - √The resultant Doppler FMs of the two VCOs are out of phase and equal in magnitude, canceling each other out in the MIL process
 - x The complexity of the system makes the actual measurement difficult







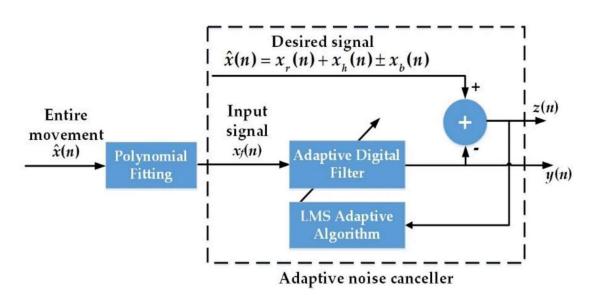


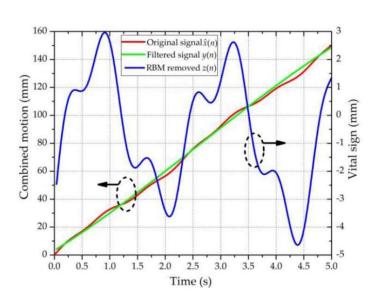


Literature Review (2/3)



- Adaptive Noise Cancellation (ANC) [2]
 - ✓ Polynomial fitting method to extract vital signs in the large-scale RBM
 - x Not choosing the correct step-size affects convergence speed





[2] Z. Yang, H. Shi, S. Zhao, X. Huang, "Vital Sign Detection during Large-Scale and Fast Body Movements Based on an Adaptive Noise Cancellation Algorithm Using a Single Doppler Radar Sensor," in Sensors, vol. 20, no. 15, pp.4183, 2020.



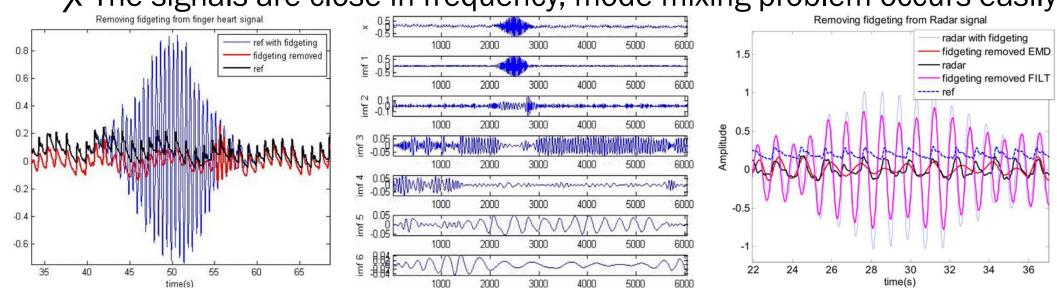




Literature Review (3/3)



- Empirical Mode Decomposition (EMD) [3][4]
 - ✓ EMD was applied to removing fidgeting motion
 - x The signals are close in frequency, mode mixing problem occurs easily



[3] I. Mostafanezhad, O. Boric-Lubecke, V. Lubecke and D. P. Mandic, "Application of empirical mode decomposition in removing fidgeting interference in doppler radar life signs monitoring devices," in 2009 Annu Int Conf IEEE Eng Med Biol Soc., pp. 340-343, 2009.

[4] C. -Y. Huang, G. -W. Fang, H. -R. Chuang and C. -L. Yang, "Clutter-Resistant Vital Sign Detection Using Amplitude-Based Demodulation by EEMD-PCA-Correlation Algorithm for FMCW Radar Systems," 2019 EuMC, Paris, France, pp. 928-931, 2019.







Theory Analysis (1/6)



The reflected signal from target is received by the FMCW

$$S_B(t) = A_d \exp\left(j\left(2\pi f_b t + \frac{4\pi f_c R(\tau)}{c} + \Delta\phi_0(t)\right)\right)$$

$$+A_c \exp\left(j\left(2\pi f_{bc} t + \frac{4\pi f_c R_c(\tau)}{c} + \Delta\phi_c(t)\right)\right)$$

$$(1)$$

where

 A_d , A_c : the amplitudes of the beat signal from target and non-stationary clutter

 f_b , f_{bc} : the beat frequency of the target and non-stationary clutters

 $R(\tau)$, $R_c(\tau)$: the distances of the radar system relative to the target and the non-stationary clutter

 ϕ_0 , ϕ_c : residual phase noise







Theory Analysis (2/6)



 To extract the phase information, the signal from the target range bin

$$S_B(\tau) = A_d \exp(j\varphi_t) + A_c \exp(j\varphi_c)$$
 (2)

Vital signs

$$\varphi_t = j \frac{4\pi f_c \cdot R(\tau)}{c}$$

Non-stationary Clutter

$$\varphi_c = j \frac{4\pi f_c \cdot R_c(\tau)}{c}$$

where

 A_d , A_c : the amplitudes of the beat signal from target and non-stationary clutter

 $R_c(\tau)$: distance and vibration of non-stationary clutter



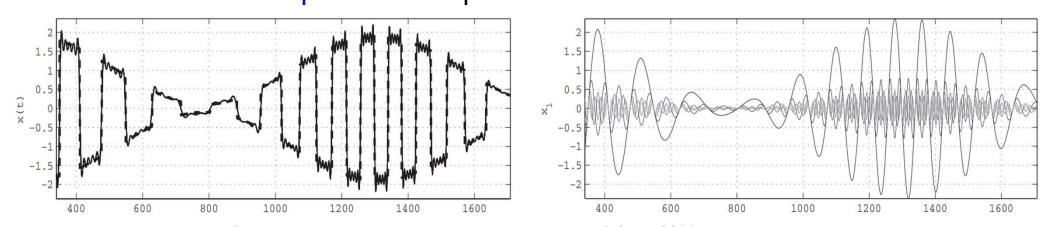


Theory Analysis (3/6)



Characteristics of HVD

- To HVD method, dedicated to the problem of decomposition of nonstationary vibration [5]
- The first component separated from the initial vibration contains the varying highest amplitude. The residual signal contains information of other lower amplitude components



[5] Feldman, Michael. Hilbert transform applications in mechanical vibration. John Wiley & Sons, 2011.







Theory Analysis (4/6)



HVD is based on Hilbert Transform (HT) and analytical signal

analytic signal

$$X(t) = x(t) + i\tilde{x}(t) = A(t)e^{j\psi(t)}$$
 (3) \tilde{x} : the HT of $x(t)$

instantaneous amplitude $A(t) = \sqrt{x(t)^2 + \tilde{x}(t)^2}$

$$A(t) = \sqrt{x(t)^2 + \tilde{x}(t)^2}$$

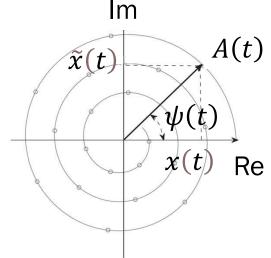
(4)

instantaneous phase
$$\psi(t) = \arctan \frac{\tilde{x}(t)}{x(t)}$$

(5)

instantaneous frequency $\omega(t) = \dot{\psi}(t)$

(6)



[5] Feldman, Michael. Hilbert transform applications in mechanical vibration. John Wiley & Sons, 2011.

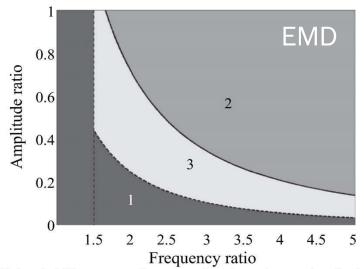


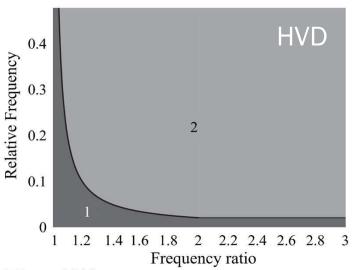
Theory Analysis (5/6)



HVD frequency resolution

- HVD decomposes the initial signal to slow varying part and faster varying part
- HVD with better frequency resolution capacity, decompose frequencies closer than EMD [5]





[5] Feldman, Michael. Hilbert transform applications in mechanical vibration. John Wiley & Sons, 2011.







Theory Analysis (6/6)



Synchronous demodulation

– To extract the amplitude of a known frequency by multiplying the initial component by a reference signal $r(t) = \cos(\int \omega_r(t) dt)$

$$x(t) = \sum A_l(t) \cos \left(\int \omega_l(t) dt + \varphi_l \right) \quad (7) \quad \tilde{x}(t) = \sum A_l(t) \sin \left(\int \omega_l(t) dt + \varphi_l \right) \quad (8)$$

$$x_l(t) = x(t) \times r(t) = \frac{1}{2} A_l(t) \left[\cos(\varphi_l(t)) + \cos(\int (\omega_l(t) + \omega_r(t)) dt + \varphi_l(t)) \right]$$
 (9)

$$\tilde{x}_l(t) = \frac{1}{2} A_l(t) \left[-\sin(\varphi_l(t)) - \sin(\int (\omega_l(t) + \omega_r(t)) dt + \varphi_l(t)) \right]$$
(10)

$$A_l(t) = \sqrt{x_l(t)^2 + \tilde{x}_l(t)^2}$$
 (11) $\varphi_l(t) = \arctan \frac{x_l(t)}{\tilde{x}_l(t)}$ (12)

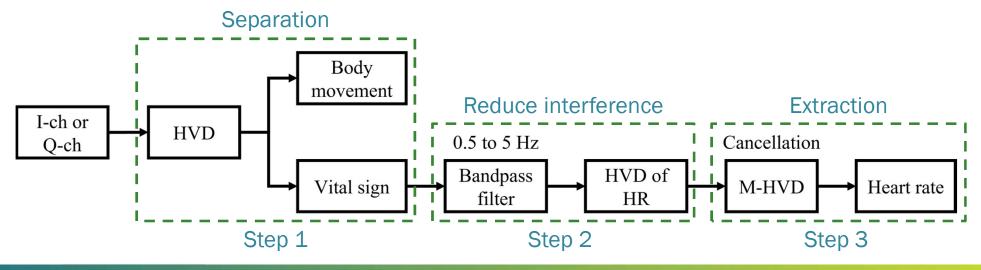




Proposed Method (1/3)



- The proposed algorithm consists of three steps:
 - 1. Separates the RBM from the vital signs
 - 2. Reduce interference from the non-stationary clutter and extract the heartbeat
 - 3. Reduce the error rate, interference signal and improve SNR





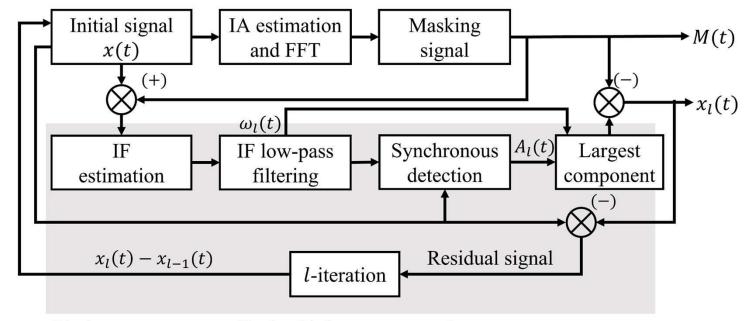




Proposed Method (2/3)



- Block diagram of masking signal HVD. The gray area is HVD
 - HVD: separation of nonstationary vibration into simple components
 - M-HVD: improve the signal separation performance



IA: instantaneous amplitude; IF: instantaneous frequency







Proposed Method (3/3)



Masking signal HVD (M-HVD)

- The maximum amplitude FFT of the initial signal is proposed as masking signal to improve the non-stationary synthetic signals [6]
- The initial signal is added and the new signal $x_m(t) = x(t) + M(t)$

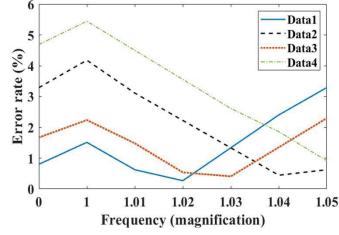
$$M(t) = A_m \sin(2\pi f_m t)$$

 A_m is obtained as the average amplitude of $1.6 \times A(t)$

$$A(t) = \sqrt{x(t)^2 + \tilde{x}(t)^2}$$

The largest FFT spectrum amplitude is define as *f*

$$f_m = 1.02 \times f$$



[6] J. J. Ramos, J. I. Reyes and E. Barocio, "An improved Hilbert Vibration Decomposition method for analysis of low frequency oscillations," 2014 IEEE PES Transmission & Distribution Conference and Exposition - Latin America (PES T&D-LA), 2014, pp. 1-6.



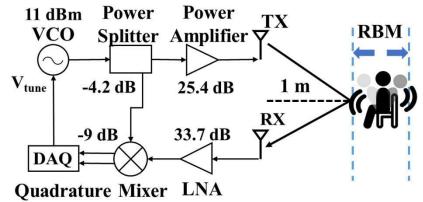


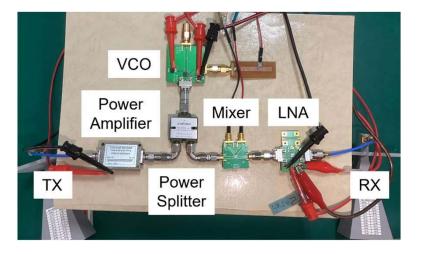


Experiment Setup



Parameter	Value
Central Modulation Frequency	24 GHz
Modulation Bandwidth	250 MHz
Pulse Repetition Interval	2 ms
Range Resolution	0.6 m
Measurement Period	60 sec
RBM velocity	1.6 $^{cm}/_{s}$







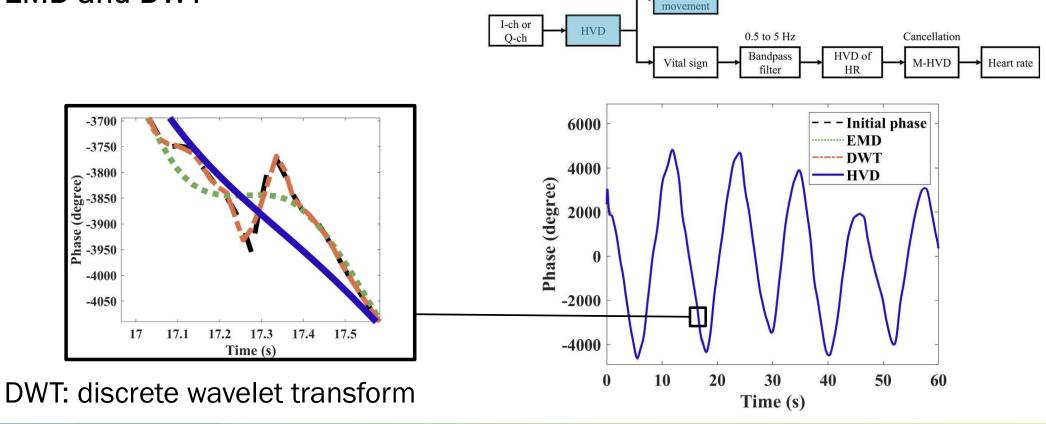






Comparison of the target phase with the decomposition following HVD,

EMD and **DWT**





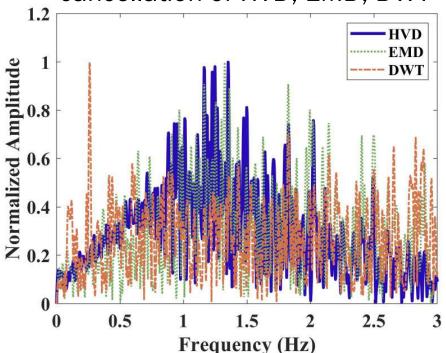


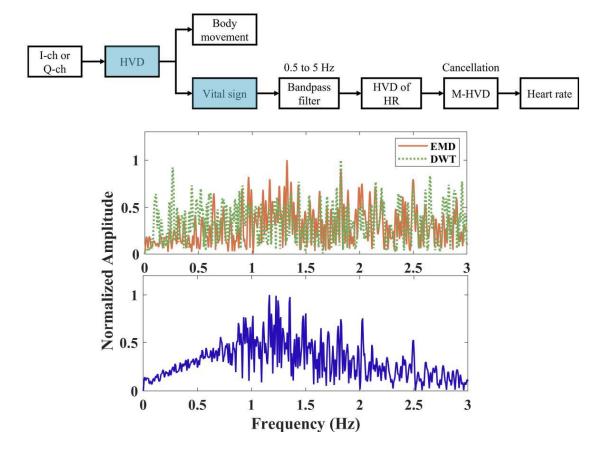




Comparison among EMD, DWT, and HVD

Phase spectrum of RBM after cancellation of HVD, EMD, DWT







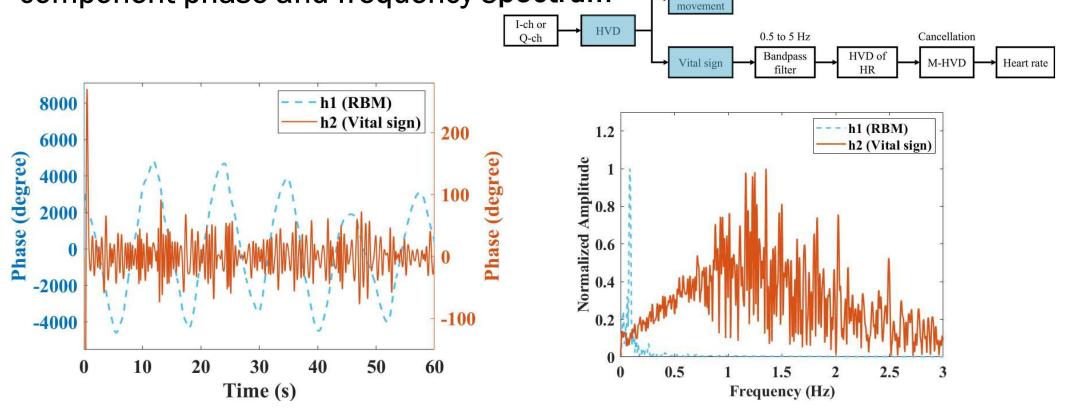






Separation of RBM signal from vital signs by first-stage HVD of the

component phase and frequency spectrum





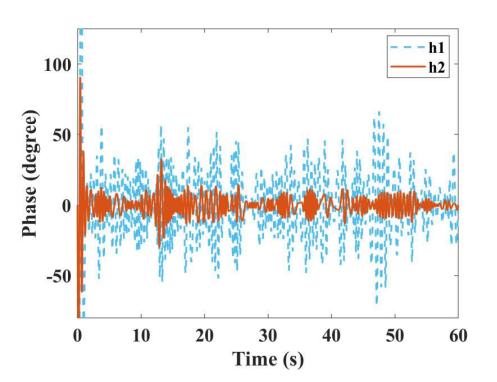


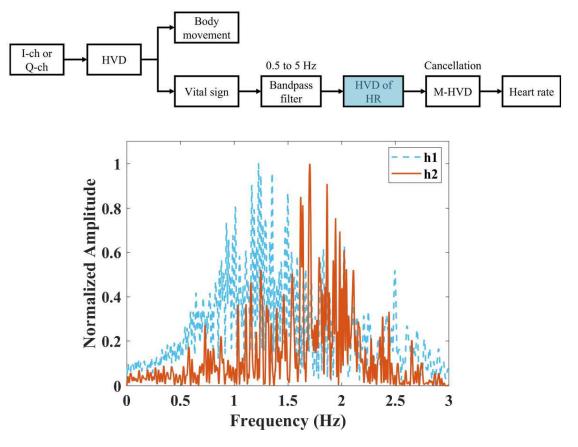




The phase and spectrum of the component after the first stage HVD is

separated by second stage HVD





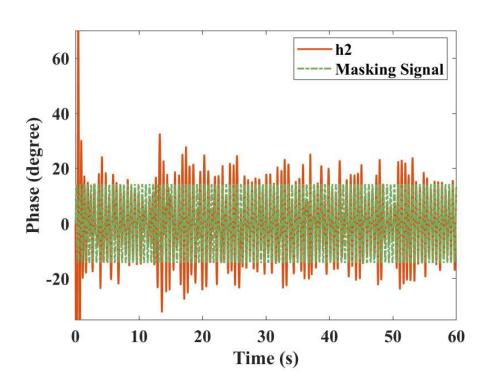


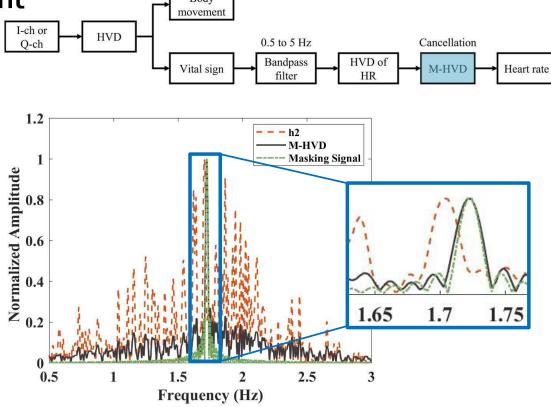




Comparison of the spectrum before and after adding the masking signal

to the second stage HVD component



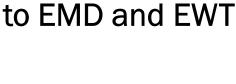


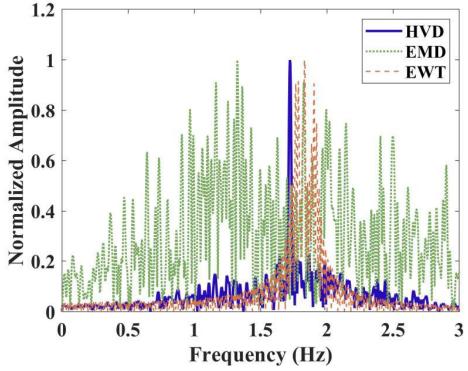






Results of frequency spectrum processed by the proposed HVD compared





EWT: empirical wavelet transform







Measurement Results



 In addition to the comparison of spectrum results, the relative error, SNR and computational load are also used for comparison

$$SNR_{0\sim3Hz,dB} = 10\log\frac{P_{signal}}{P_{noise}}$$

SNR
$$SNR_{0\sim3Hz,dB} = 10\log\frac{P_{signal}}{P_{noise}}$$
 Average relative error
$$Error_{HR}(\%) = \frac{1}{N} \sum_{k=1}^{N} \frac{\left|HR_{HVD,k} - HR_{Ref,k}\right|}{HR_{Ref,k}} \times 100\%$$

Algorithm	HR Error (%)	SNR (dB)	Processing Time (s)
EMD	46.22	7.02	0.083
EWT	2.75	19.36	0.066
HVD	2.61	23.04	0.633
This work	1.64	27.73	0.883





Measurement Results



Literature Comparison

	System	Method	Range	HR Error
Liu et al. [7]	77 GHz	DRSEPK	1 m	4.68 %
	FMCW	DROEPN		
Yin et al. [8]	8.5 GHz	HEAR	1 ~ 2 m	6.15 %
	IR-UWB			
This work	24 GHz	HVD	1 m	1.64 %
	FMCW			

[7] L. Liu, S. Zhang and W. Xiao, "Non-Contact Vital Signs Detection Using mm-Wave Radar During Random Body Movements," 2021 IEEE 16th Conference on Industrial Electronics and Applications (ICIEA), 2021, pp. 1244-1249.
[8] Yin, W.; Yang, X.; Li, L.; Zhang, L.; Kitsuwan, N.; Oki, E. HEAR: Approach for Heartbeat Monitoring with Body Movement





Compensation by IR-UWB Radar. Sensors 2018, 18, 3077



Conclusion



- Proposed an HVD algorithm for non-contact vital sign detection using FMCW radar in large-scale RBM
- HVD effectively separates the large-scale RBM from the vital signs
- Result of signal processing have the average relative error 1.64%, and SNR improvement of 8.3 dB compared with EWT
- Advantage of the proposed algorithm:
 - High accuracy
 - High SNR
 - Low computational load









Thanks for your attention.

Questions?

Feel free to contact us!

Pei-Ling Cheng *: n26100375@gs.ncku.edu.tw

Prof. Chin-Lung Yang: cyang@mail.ncku.edu.tw



