



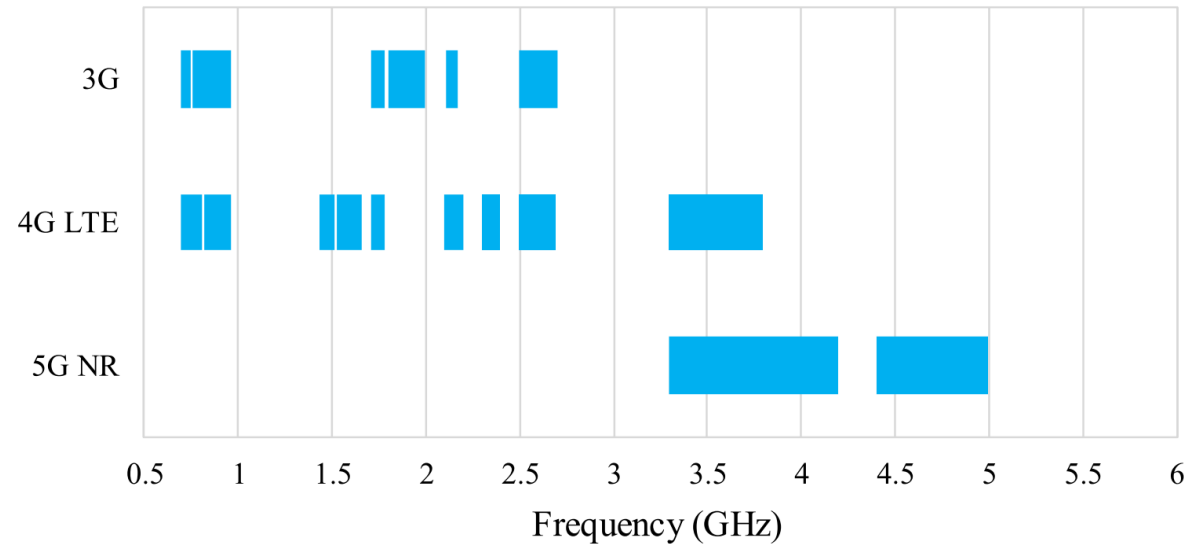
Tu3D-5

Design of Highly-Efficient Dual-Band GaN HEMT Power Amplifier With Dual-Class E/F-1 Operation

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- **Motivation**
- **Proposed Structure and Design**
- **Verification Results**
- **Conclusion**

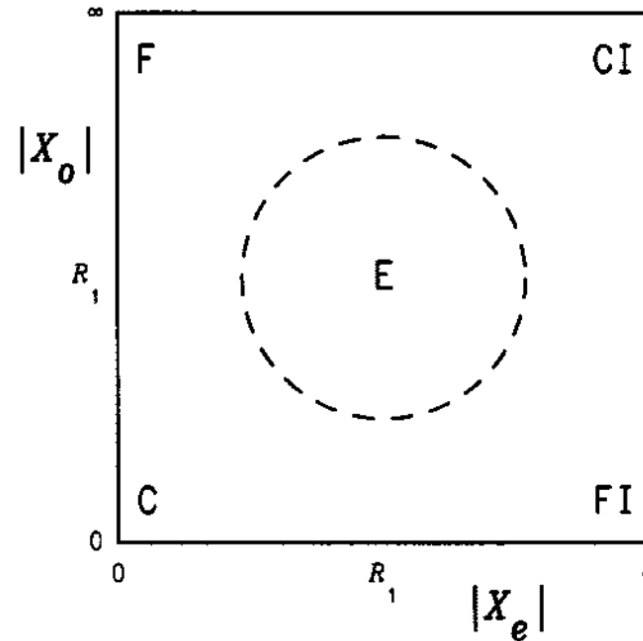
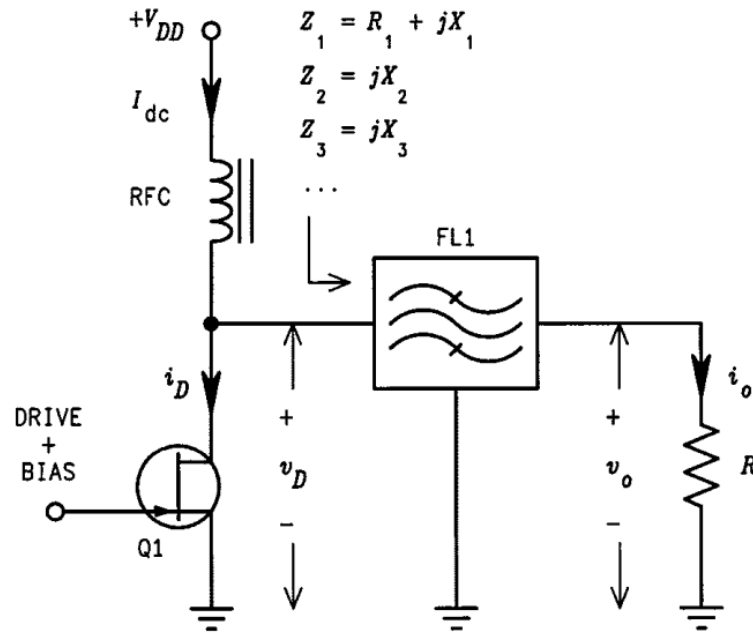
- **Wireless communication spectra – the sub-6 GHz**
 - scattering widely, best compromise between capacity and coverage



Sub-6-GHz frequency bands for 3G, 4G LTE, and 5G NR [1]

- **Multi-band mode for RF transmitters**
 - reconfigurable and highly-integrated solution, low cost.

- **RF Power Amplifier (PA)– the sub-6 GHz**
 - most expensive, challenging
 - performance matrices: drain efficiency (DE), power-added efficiency (PAE), output power, linearity, and size
 - high DE/PAE: priority in design
- **High-PAE PA**
 - switch-mode PAs: class D, class E
 - harmonic-tuned PAs: class J, class F/inverse class F (class F-1)



X_o : odd harmonic reactance
 X_e : even harmonic reactance

Generic PA structure and class theoretical classification based on harmonic impedance [2]

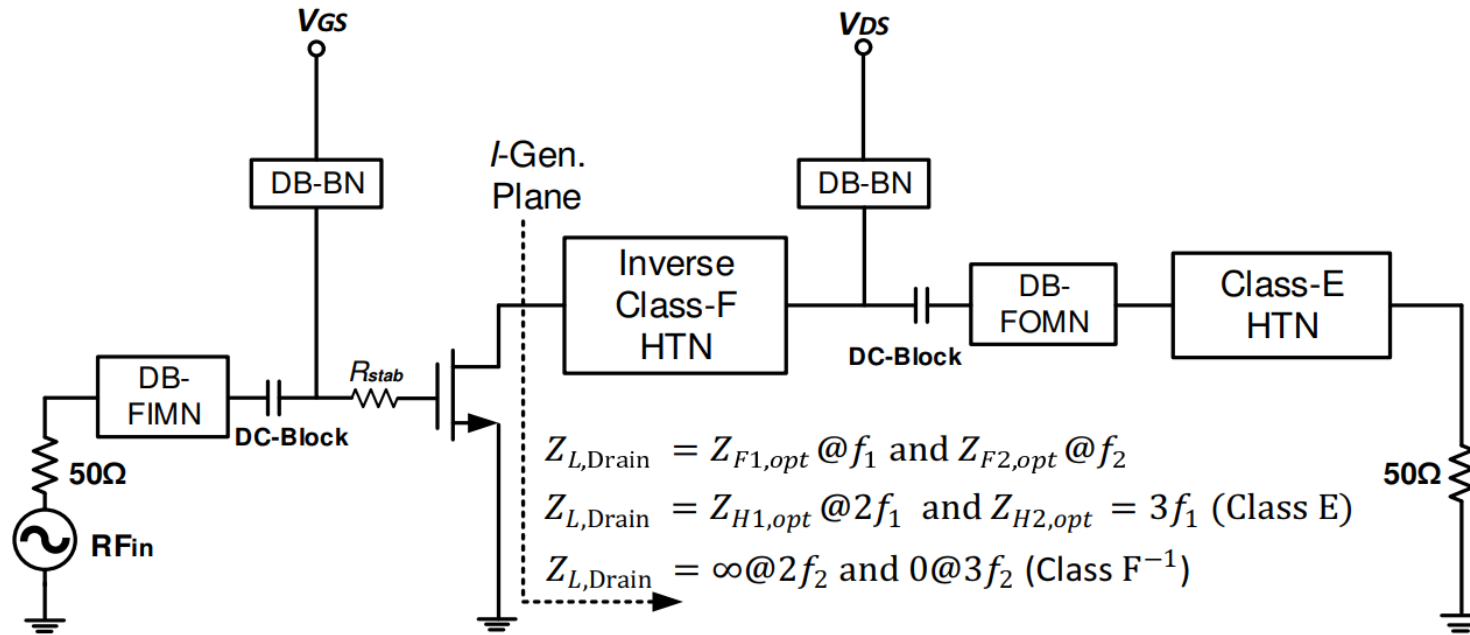
- **Class F/F-1:** even/odd harmonics are low, odd/even harmonics are high
- **Class E:** all harmonic reactances are comparable in magnitude to the fundamental-frequency load resistance

- Comparison between class E and class F/F-1 modes [3]

| Class E | Class F/F-1 |
|--|--|
| High Efficiency (up to 100%) | High Efficiency (up to 100 %) |
| Harmonic requirements are more forgiving → simple load network | Harmonic requirements are more rigorous → complicated load network |
| Subject to operating frequency limitation | No operating frequency limitation |

- Dual-band (DB) operation: class-E for low band, class F-1 for high band → high PAE and uncomplicated design.

Proposed Structure and Design

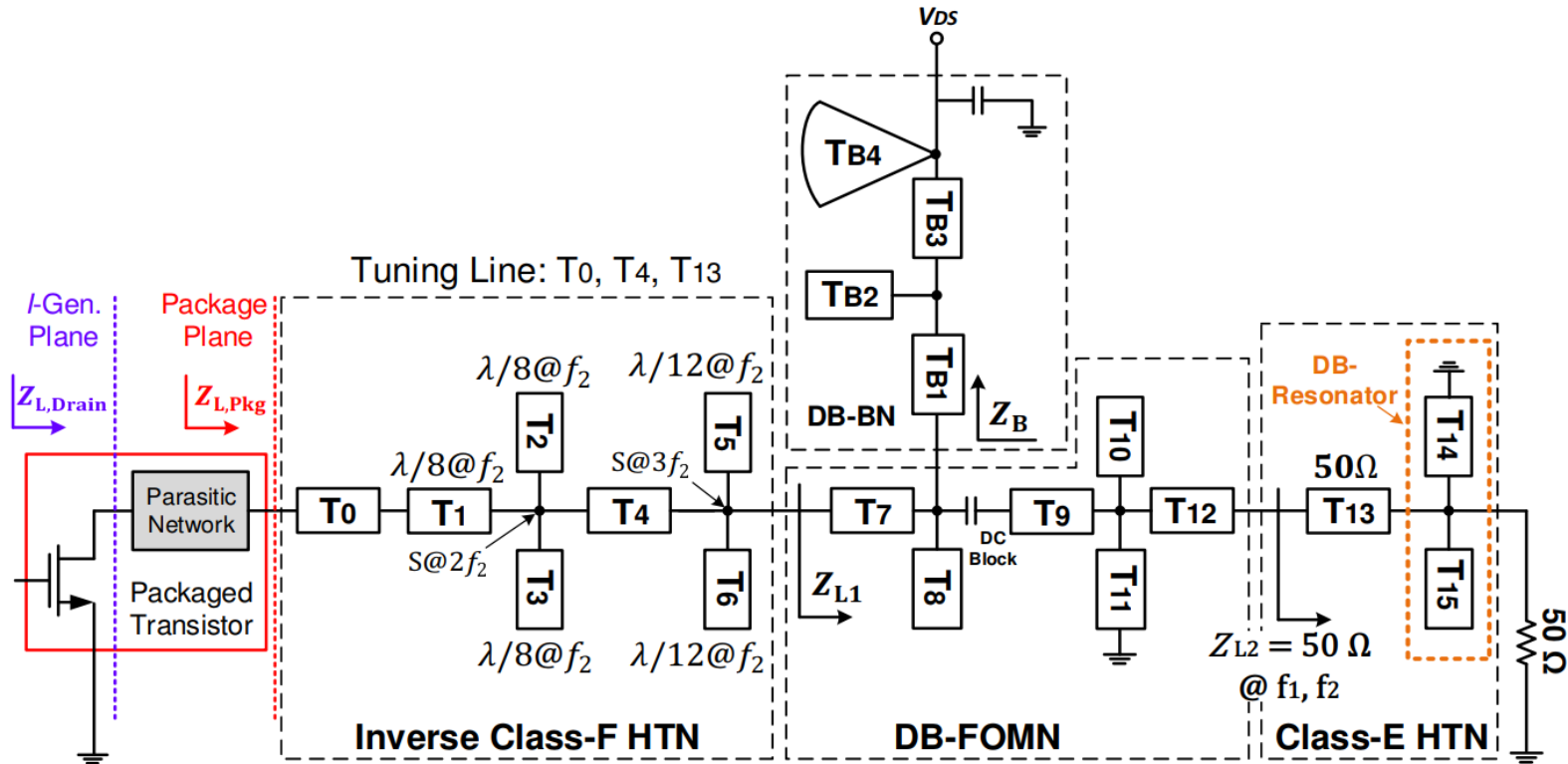


- ✓ HTN: Harmonic Termination Network
- ✓ DB: Dual-band
- ✓ FOMN: Fundamental Output Matching Network
- ✓ FIMN: Fundamental Input Matching Network
- ✓ DB-BN: Dual-Band Biasing Network

Proposed structure for dual-class E/F-1 operation

- **Harmonic Control:** Inverse class F HTN, class-E HTN.
- **Fundamental Matching:** DB-FOMN, DB-FIMN
- **DC Biasing:** DB-BN

Proposed Structure and Design

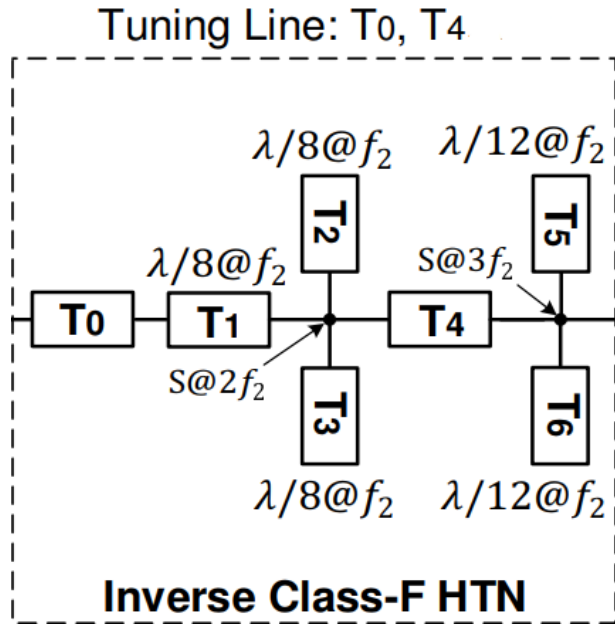


Detail load structure for dual-class E/F-1 operation

- Implementation based on transmission lines
- Active device: packaged transistor

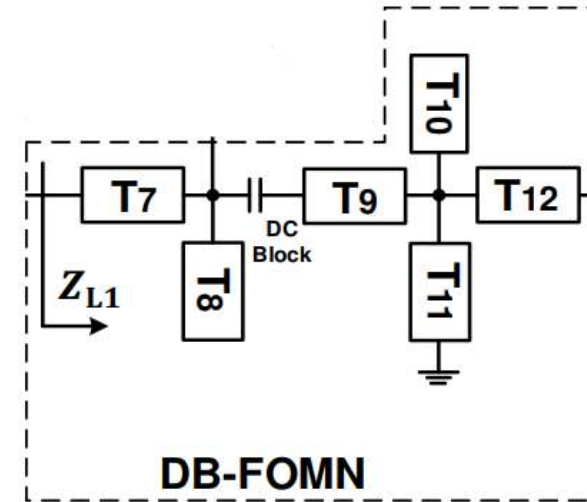
- Inverse class F HTN
 - open circuit for $2f_2$, short circuit for $3f_2$ at I -Gen plane
 - considering effects of parasitic network, isolated with others
- DB-FOMN: – DB matching to $50\ \Omega$
- DB-BN: – shorted at DC and open at fundamental frequencies
- Class-E HTN
 - as a $50\ \Omega$ - $50\ \Omega$ transformer at the fundamentals
 - Class-E harmonic termination at f_1 , does not affect to others

- Inverse Class-F HTN [4]



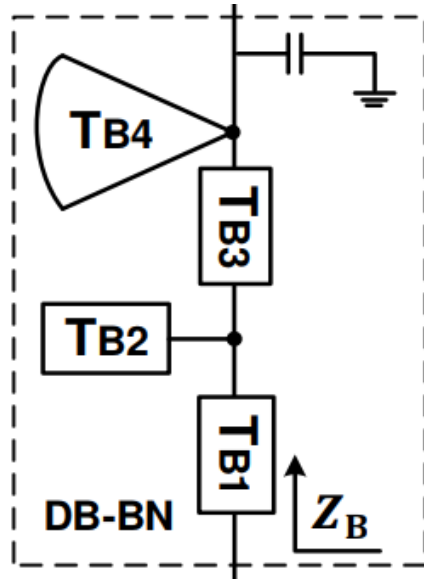
- Including two shunt stubs in each of two arms
- Based on tuning mechanism

- DB-FOMN [5]



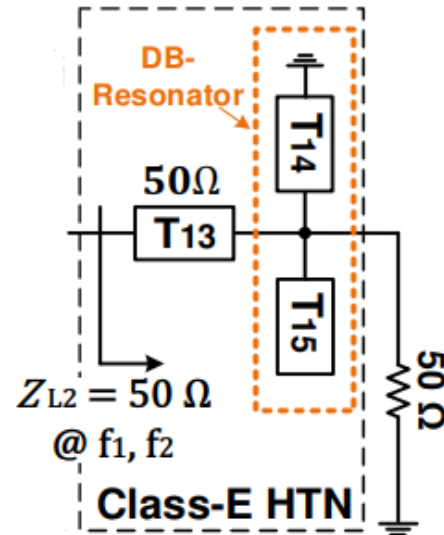
- matching fundamental optimal impedance Z_{L1} to 50Ω

- DB-BN [6]



– Z_B : zero at DC,
infinite at f_1, f_2

- Class-E HTN [5]

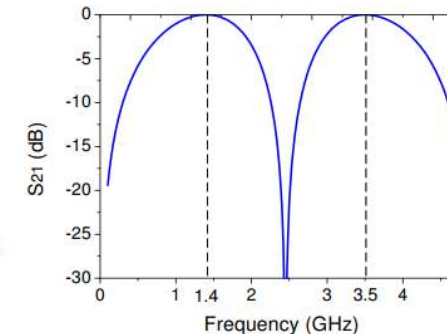
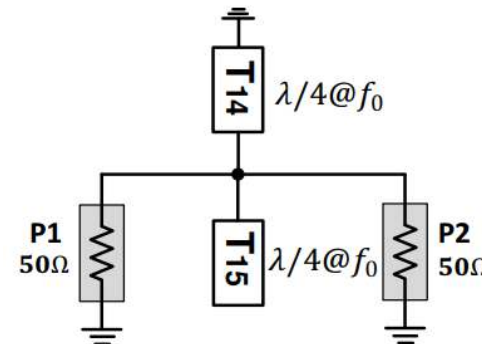


- Including a dual-band resonator and a 50 Ω tuning transmission line

$$Z_{14} = \frac{1}{4f_0 C_0} \sec^2\left(\frac{\pi}{2} \times \frac{f_2 - f_1}{f_2 + f_1}\right)$$

$$Z_{15} = \frac{1}{4f_0 C_0} \operatorname{cosec}^2\left(\frac{\pi}{2} \times \frac{f_2 - f_1}{f_2 + f_1}\right),$$

- Adding T_{13} does not influence the fundamental impedance, harmonics of f_1 are modified with its length



- **Design Process - Three Steps**
 - Step 1: first realizing class F-1 HTN, yielding class F-1 operation at the I -generation plane.
 - Step 2: then designing DB-FOMN, correctly matching fundamental optimal impedance to $50\ \Omega$. At this step, adding a DB-BN which does not affect to the matching performance.
 - Step 3: class E HTN follows the DB-FOMN, acting as a $50\ \Omega$ - $50\ \Omega$ transformer and only influencing to the harmonics of f_1 .

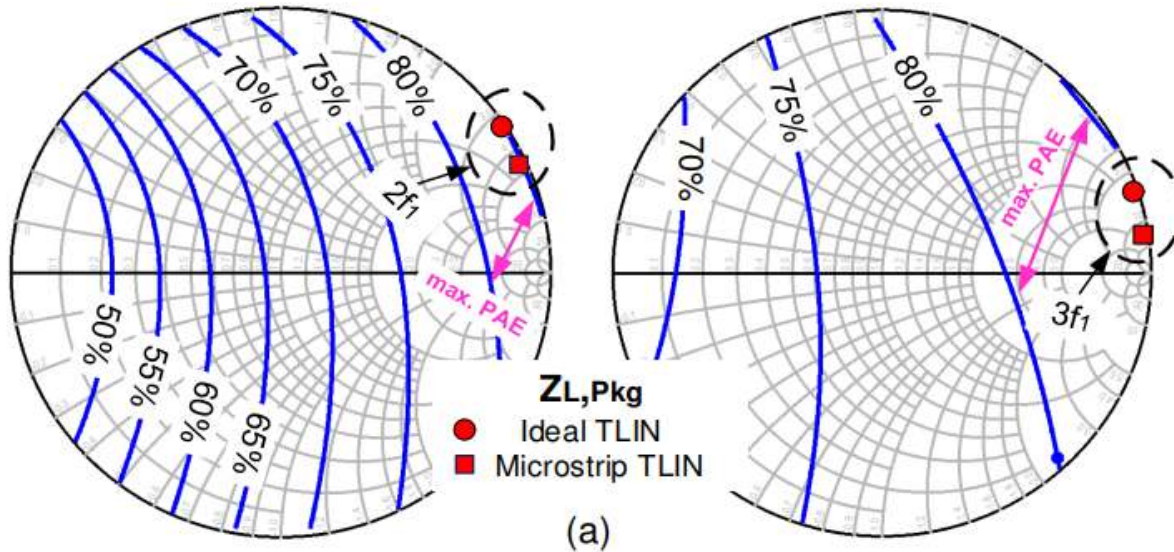
Verification Results

- Active Device: 5-W Cree transistor CGH40006P
- Operating Frequency: $f_1=1.4$ GHz, $f_2=3.5$ GHz
- Biasing Voltage: $V_{GS}=-3.2$ V, $V_{DS}=28$ V

| TLIN | T_0 | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 |
|-----------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| Z (Ω) | 90 | 90 | 120 | 120 | 90 | 120 | 120 | 90 | 90 | 126.4 |
| θ ($^\circ$) | 43.3 | 45 | 45 | 45 | 54.1 | 30 | 30 | 10 | 60 | 24.6 |
| f (GHz) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 1.4 |
| TLIN | T_{10} | T_{11} | T_{12} | T_{13} | T_{14} | T_{15} | T_{B1} | T_{B2} | T_{B3} | T_{B4} |
| Z (Ω) | 75.7 | 106.3 | 115.5 | 50 | 41.7 | 65.6 | 90 | 90 | 90 | |
| θ ($^\circ$) | 50.2 | 51.2 | 56.4 | 19 | 90 | 90 | 90 | 90 | 86 | 90 |
| f (GHz) | 1.4 | 1.4 | 1.4 | 1.4 | 2.45 | 2.45 | 3.5 | 3.5 | 3.5 | 1.4 |

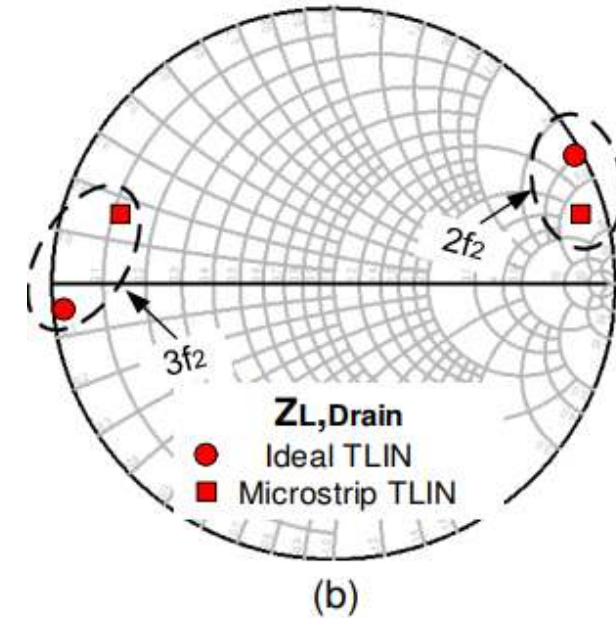
Extracted TLIN parameters for dual-class E/F-1 operation

Verification Results



Simulated PAE contours and location of $Z_{L,Pkg}$ at $2f_1$ and $3f_1$

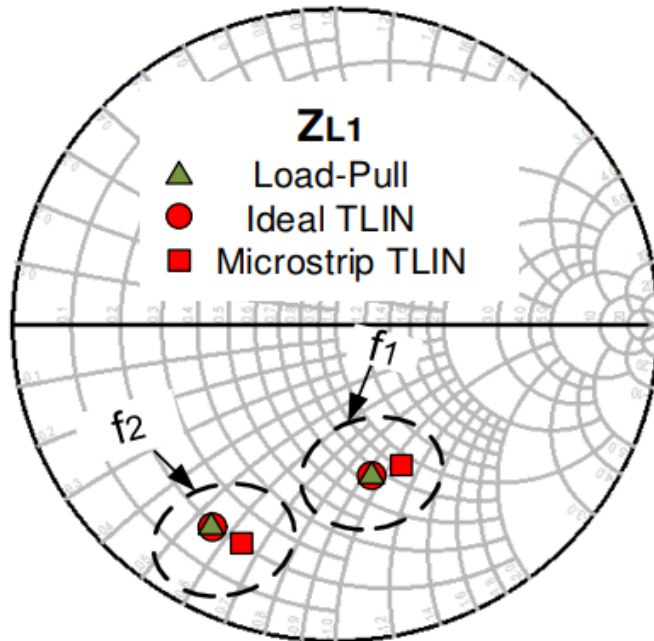
- 2nd and 3rd harmonics are located at optimal regions
- Efficient class-E operation at f_1



Simulated location of $Z_{L,Drain}$ at $2f_2$ and $3f_2$

- Second harmonic spreads near the open-circuit point while third harmonic resides close to the short-circuit region.
- Reliable class F-1 operation at f_2 .

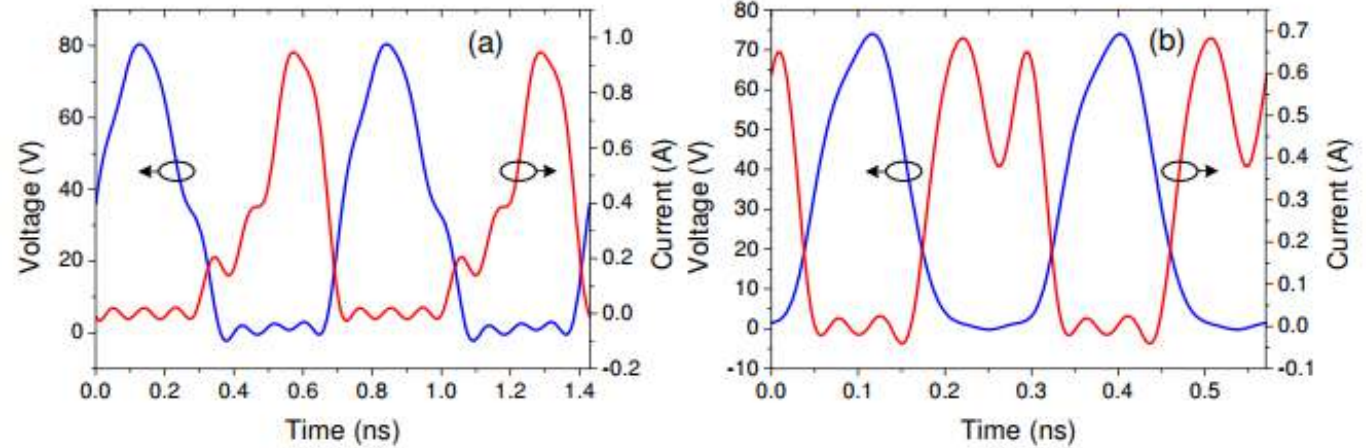
Verification Results



(c)

Simulated fundamental impedance location of Z_{L1} at f_1 and f_2

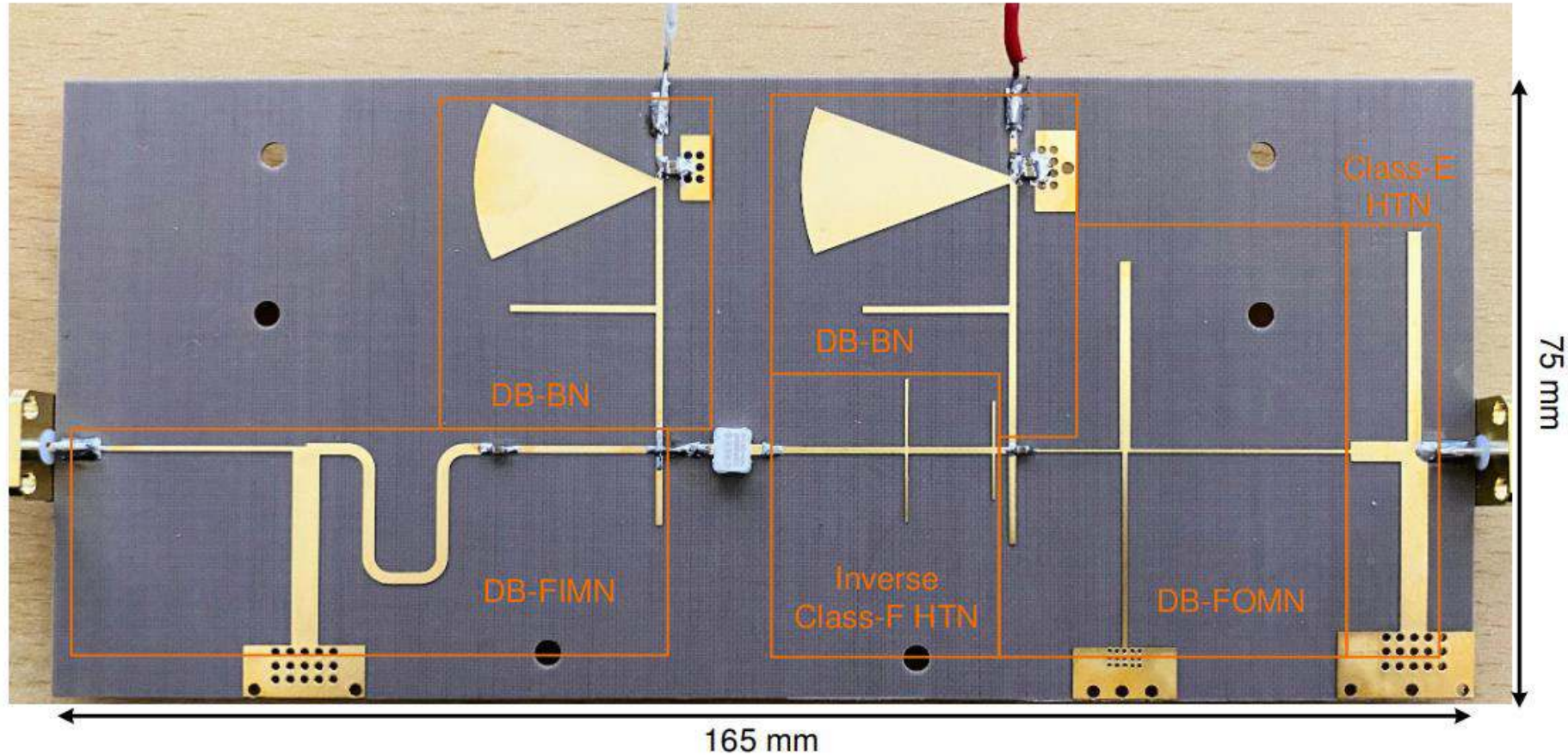
- Good agreement between load-pull and circuit simulations.



Simulated intrinsic drain waveforms of voltage and current at (a) f_1 and (b) f_2

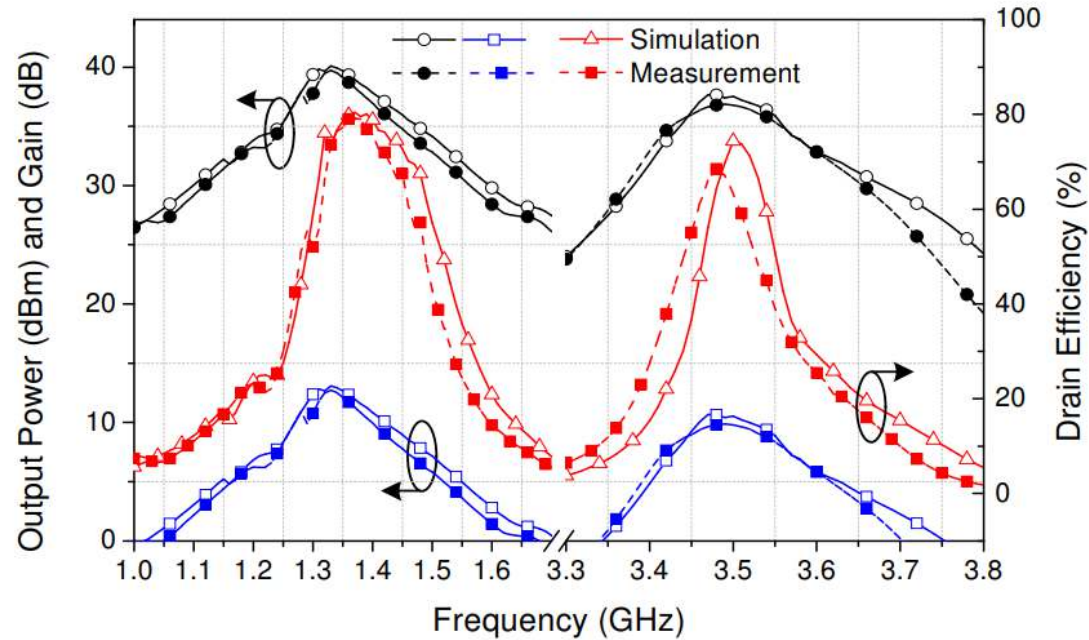
- Class E waveforms at f_1 .
- Inverse Class F waveforms at f_2 .

Verification Results



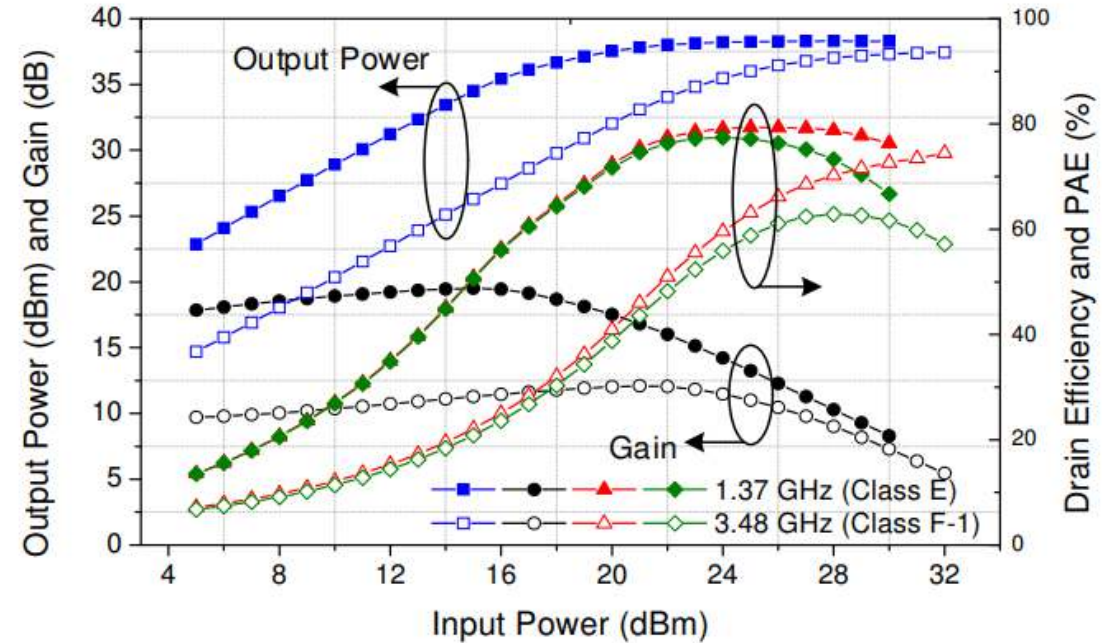
Photograph of the fabricated prototype on Taconic TLY-5 substrate ($\epsilon_r = 2.2$ and $\tan\delta = 0.0009$)

Verification Results



Simulated and measured drain efficiency, output power, gain versus frequency at an input power of 27 dBm.

- Measured peak efficiency: 79.2% at 1.37 GHz, 68.5% at 3.48 GHz.
- Output Power: 38.3 dBm at 1.37 GHz, 36.8 dBm at 3.48 GHz



Measured efficiency, PAE, output power, gain versus input power.

- Highest PAE: 77.4% at 24 dBm for 1.37 GHz; and 62.9% at 28 dBm for 3.48 GHz.

- This work presents a high efficiency DB PA with low design complexity
 - Dual-class E/F-1 strategy: class E operation for low band and class F-1 operation for high band
 - A novel structure with its design process: realizing the dual-class E/F-1 operation
 - Verification: simulation and measurement using a packaged transistor

- [1] H. Liu, C. Zhai and K. M. Cheng, "Novel Dual-Band Equal-Cell Doherty Amplifier Design With Extended Power Back-Off Range," *IEEE Trans. Microw. Theory Techn.*, vol. 68, no. 3, pp. 1012-1021, March 2020.
- [2] F. H. Raab, "Class-E, Class-C, and Class-F power amplifiers based upon a finite number of harmonics," *IEEE Trans. Microw. Theory Techn.*, vol. 49, no. 8, pp. 1462-1468, Aug. 2001.
- [3] K. Chen and D. Peroulis, "Design of Highly Efficient Broadband Class-E Power Amplifier Using Synthesized Low-Pass Matching Networks," *IEEE Trans. Microw. Theory Techn.*, vol. 59, no. 12, pp. 3162-3173, Dec. 2011, doi: 10.1109/TMTT.2011.2169080.
- [4] Young Yun Woo, Youngoo Yang and Bumman Kim, "Analysis and experiments for high-efficiency class-F and inverse class-F power amplifiers," *IEEE Trans. Microw. Theory Techn.*, vol. 54, no. 5, pp. 1969-1974, May 2006.
- [5] D.-A Nguyen and C. Seo, "A high-efficiency design for 5-W 2.4/5.8 GHz concurrent dual-band class-E power amplifier," *Microw. Opt. Technol. Lett.*, vol. 63, no. 4, pp. 1083–1090, Apr. 2021.
- [6] Q. -F. Cheng, H. -P. Fu, S. -K. Zhu and J. -G. Ma, "Two-stage high-efficiency concurrent dual-band harmonic-tuned power amplifier," *IEEE Trans. Microw. Theory Techn.*, vol. 64, no. 10, pp. 3232-3243, Oct. 2016.

Thank you for your attention!

Q & A