

WE1A-4

Inter-Satellite Phase and Frequency Synchronization for Software-Defined CubeSat Radio Subsystems

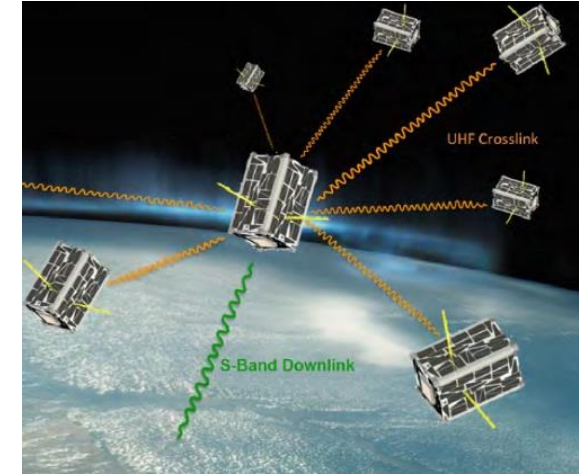
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Cooperating Satellites

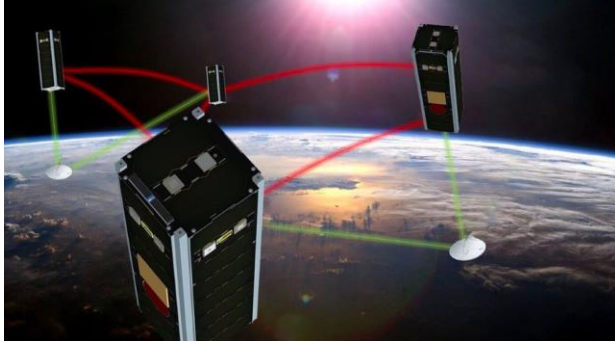
- Cooperating satellites
 - Being used for +12 years
 - Recent interest: LEO small satellites
- Advantages
 - New application areas + improved mission performance
 - Cost savings + system level redundancy
- Common term: *distributed satellite system (DSS)*
- Classes of *cooperating* DSSs: *cluster, swarm, fractionate spacecraft, federated satellite system (FSS)*
- Often require ranging & synchronization, recent overview of methods in²



¹NASA Edison Demonstration of Smallsat Networks (EDSN).

²L. M. Marrero et al., "Architectures and Synchronization Techniques for Distributed Satellite Systems: A Survey", 2022.

NETSAT¹



- 4x 3U CubeSats (DSS cluster)
- Objective: analyze different 3D formation topologies
- Launch: 28.09.2020

CloudCT²

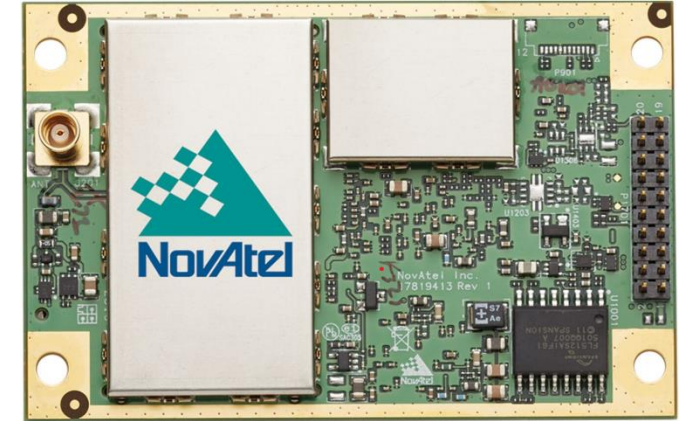


- 10x 3U CubeSats (DSS cluster)
- Objective: 3D computed tomography of clouds
- Launch planned 2024

¹Julian Scharnagl et al., “NetSat - Challenges of a Formation Composed of 4 Nano-Satellites”, 2021.

²Maximilian von Arnim et al., “The CloudCT Formation Of 10 Nano-Satellites For Computed Tomography To Improve Climate Predictions”, 2022.

- Typical solution: GNSS
 - Precision and accuracy limited
 - Orbit height limited
 - Requires additional space and energy
- Dedicated sync & ranging subsystem? Additional volume, mass, power consumption, etc.
- Motivation: implement synchronization & ranging with existing subsystems
- There is always: a *communications subsystem*



¹NovAtel OEM719 Multi-Frequency GNSS Receiver.

- *Software-defined radio*
- **Benefits, see e.g. NASA report¹**
 - Increasingly small and efficient
 - Attractive due to flexibility
- **Typical CubeSat configuration (up to C-band)**
 - 1U PCB size, standardized (e.g. PC104)
 - Analog Devices AD936x TRXs
 - SoCs (FPGA+Processor), e.g. Xilinx Zynq-7000 family
- **Commercially available: GOM Space, Alén Space, IQ Spacecom, etc.**



¹NASA, "State of the Art Small Spacecraft Technology (2022)".

²Alén Space Totem SDR.

- No CubeSat mission using SDR for (highly precise) synchronization or ranging known to the authors
- State of the Art: Prager et al.¹, two-way time transfer (TWTT) based fine synchronization and ranging
 - Application: distributed MIMO SAR
 - Requires: GPS for coarse synchronization and syntonization
- Can synchronization and ranging be implemented with COTS SDR solutions without pre-synchronization?²
- *Can we improve our previous work to bring the system towards carrier phase synchronization?*

¹S. Prager et al., “Wireless Subnanosecond RF Synchronization for Distributed Ultrawideband Software-Defined Radar Networks,” 2020.

²M. Gardill et al., “Towards Wireless Ranging and Synchronization using CubeSat Software-Defined Radio Subsystems”, 2023.

Two-Way Time Transfer

- Parameters of interest

- Time of Flight (TOF)

$$T_{\text{ToF}} = d_{A,B}/c_0$$

- Time offset

$$\Delta T_{A,B} = \phi_B - \phi_A$$

- Relative clock skew

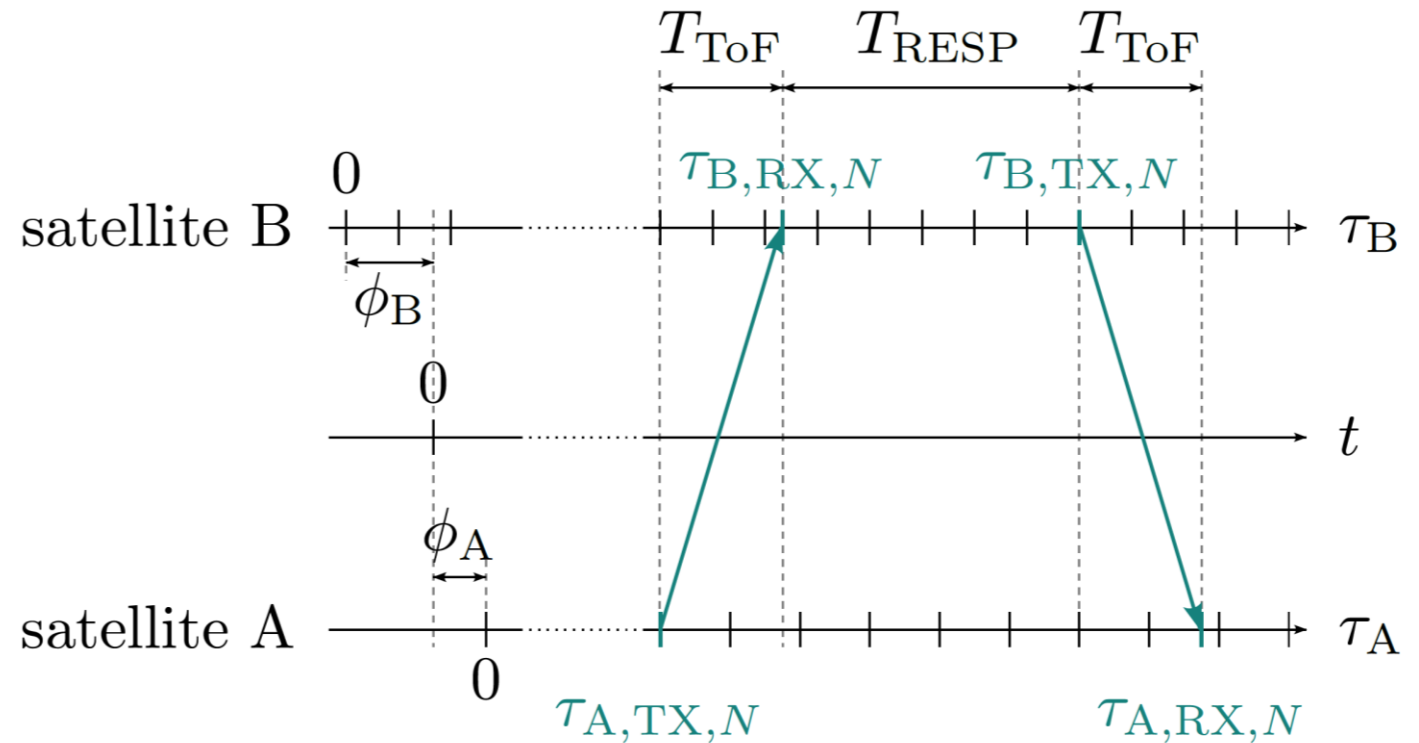
$$\alpha_A/\alpha_B$$

- Carrier phase offset

$$\gamma_{A,B}^{\text{err}} = \gamma_A - \gamma_B$$

- Clock of satellite i

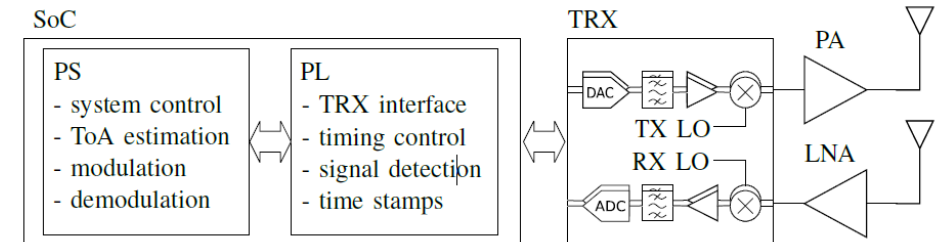
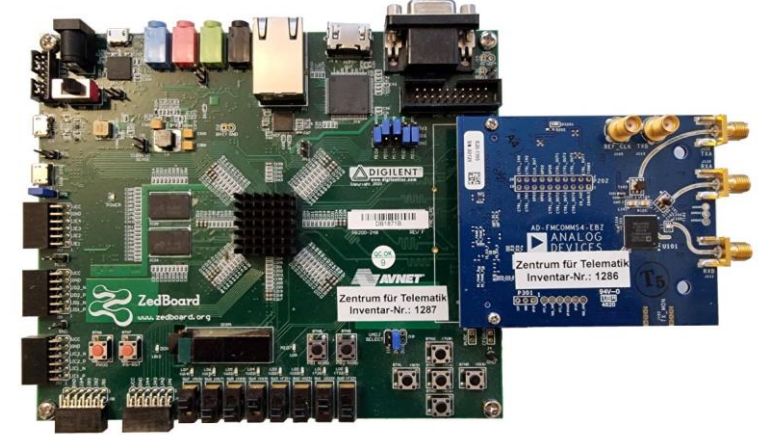
$$\tau_i = \alpha_i t + \phi_i$$



- Required to solve for parameters of interest¹
 - $\tau_{A,TX,n}, \tau_{B,RX,n}, \tau_{B,TX,n}, \tau_{A,RX,n}$
 - For two successive TWTT measurements $n \in N, N + 1$
- What the radio subsystem needs to implement
 - Highly precise time-triggered transmit for $\tau_{A,TX,n}, \tau_{B,TX,n}$
 - Time stamping for received samples
 - Highly precise time-of-arrival estimation for $\tau_{B,RX,n}, \tau_{A,RX,n}$
 - Exchange of timing information in between satellites

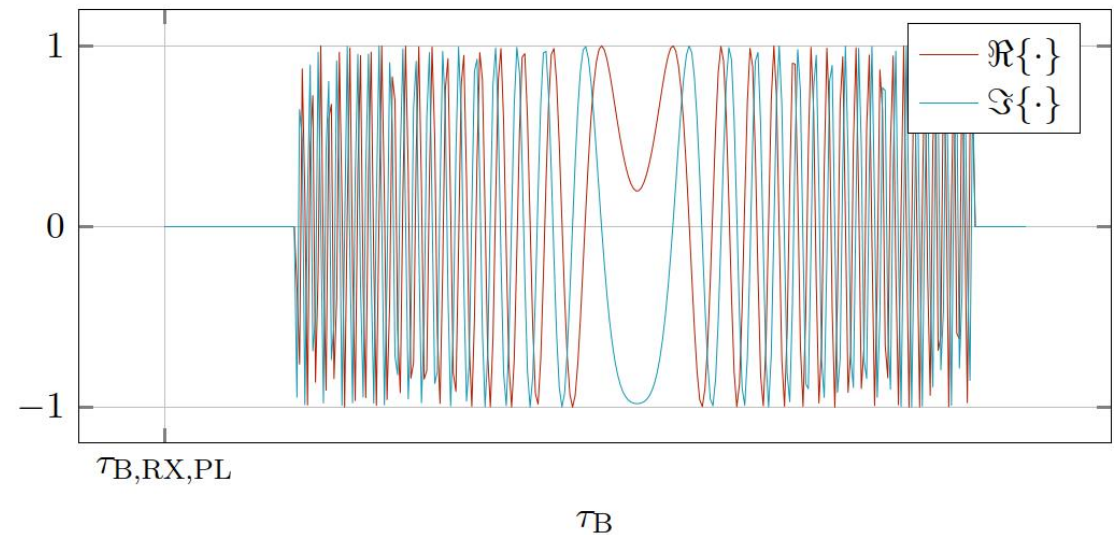
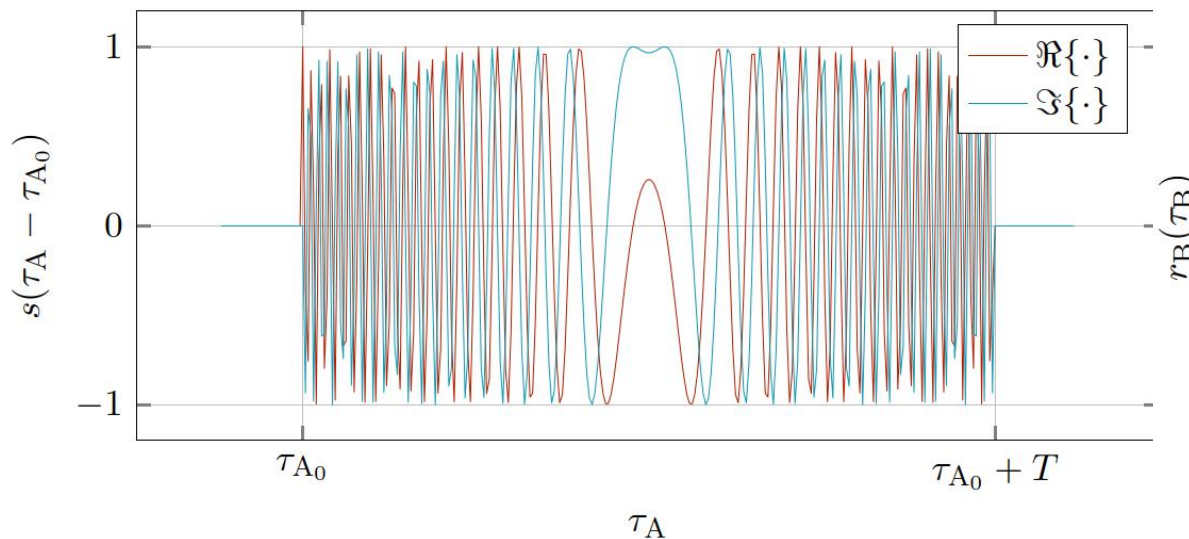
¹M. Gardill et al., “Towards Wireless Ranging and Synchronization using CubeSat Software-Defined Radio Subsystems”, 2023.

- Target platform: Alén Space Totem SDR
- Development board/Breadboard setup
 - Zedboard with Zynq-7000 SoC
 - PS: Dual-Core ARM Cortex-A9
 - PL: Artix-7 (Logic Cells, Block RAM, DSPs)
 - AD-FMCOMMS4-EBZ with AD9364 TRX
 - 1TX/1RX
 - Wideband 70 MHz - 6 GHz
 - $f_{s,max}$: 61.44 MHz; Max. Bandwidth B_{max} : 50 MHz



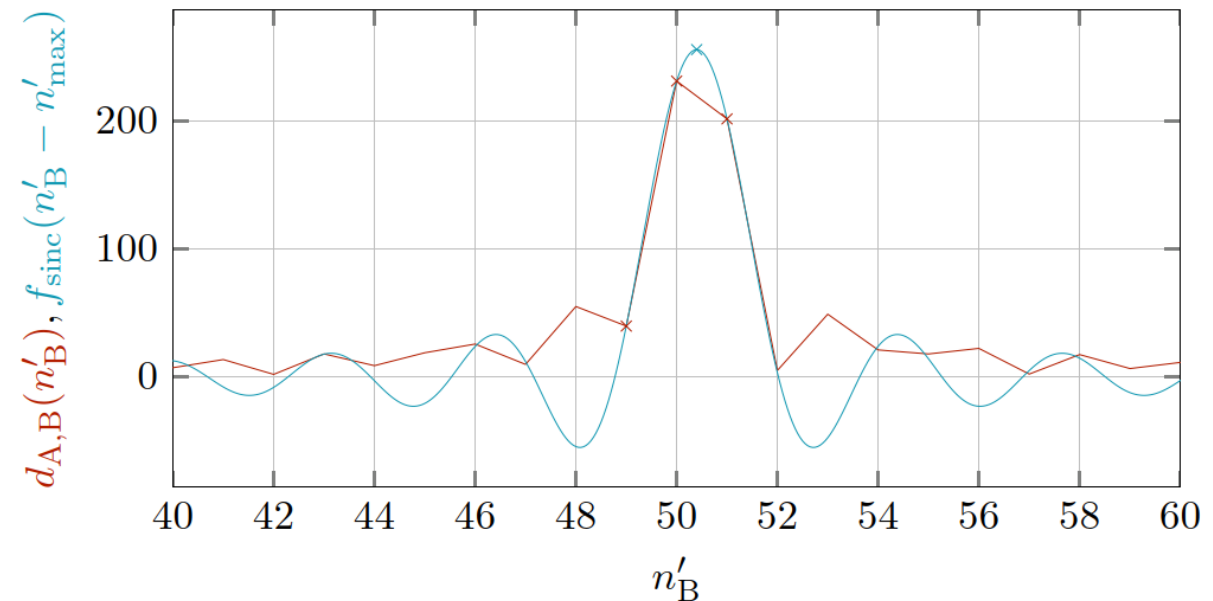
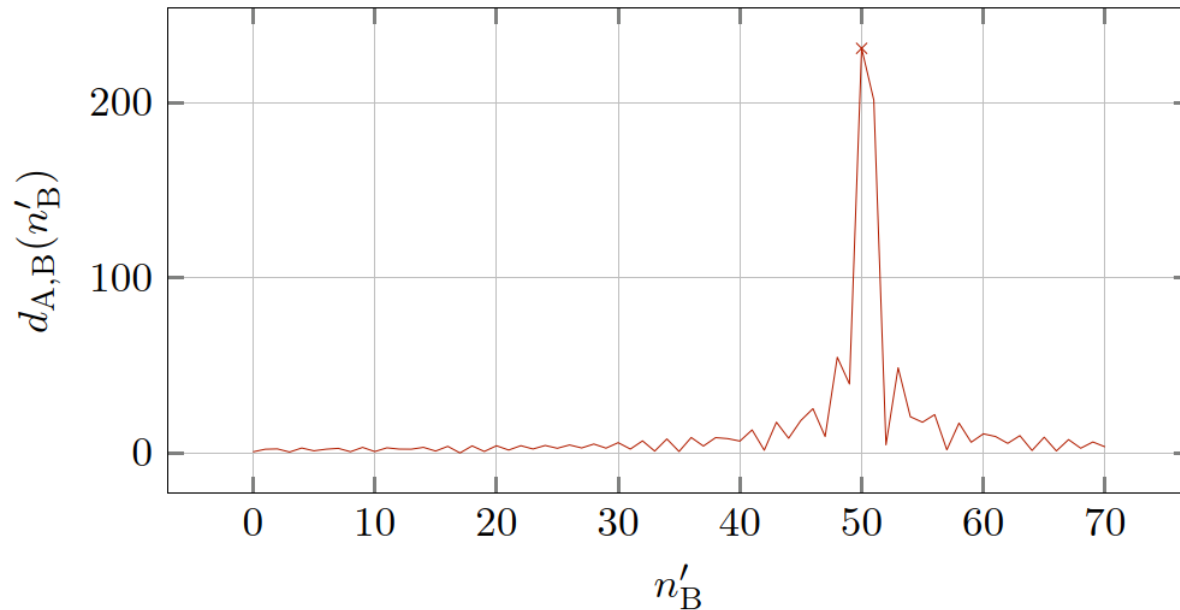
- TX signal: linear FMCW chirp, $s(t) = \exp \left(j2\pi \left(\frac{B_c f_s}{2l_c} t - \frac{B_c}{2} \right) t \right)$, $0 \leq t \leq T_c$
- RX signal model: time-scaling and delay, frequency offset, phase shift

$$r_B(\tau_B) = s \left(\frac{\alpha_A}{\alpha_B} (\tau_B - \tau_{B,RX}) \right) e^{j2\pi f_{\text{err}} \tau_B} e^{-j2\pi f_c (\alpha_B^{-1} \alpha_A (\phi_B + \tau_{B \text{ToF}}) - \phi_A)} e^{j \gamma_{A,B}^{\text{err}}}$$



- RX processing: correlation, peak detection, peak interpolation

 $\tau_{B,RX}$

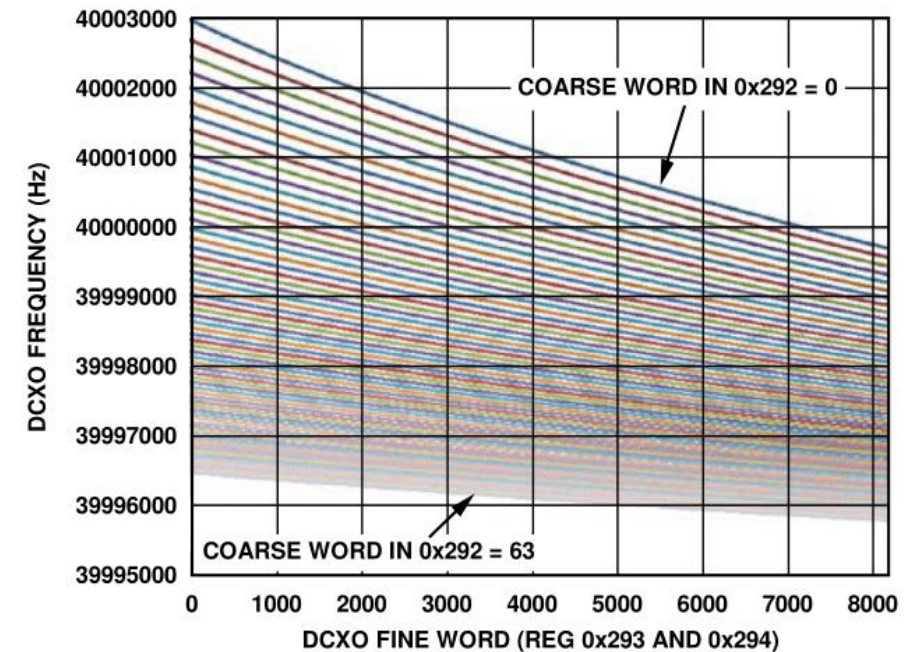


- Also use phase information from correlation: **frequency offset**, **phase shift**

$$\angle d_{A,B}(\hat{\tau}_{B,RX}) = 2\pi f_{\text{err}} \hat{\tau}_{B,RX} - 2\pi f_c \left(\frac{\alpha_A}{\alpha_B} (\phi_B + \tau_{B_{\text{ToF}}}) - \phi_A \right) + \gamma_{A,B}^{\text{err}}$$

- Idea: Use phase difference** $\Delta\varphi = \angle d_{A,B,N+1}(\hat{\tau}_{B,RX,N+1}) - \angle d_{A,B,N}(\hat{\tau}_{B,RX,N})$ from two TWTT measurements for better estimate of α_A/α_B then calculate $\gamma_{A,B}^{\text{err}}$
- Problem: Phase ambiguity** if f_{err} too big.
- Solution: DCXO**

- DCXO: digitally programmable on-chip variable capacitor + external crystal oscillator
- Coarse word + fine word
- Worst case resolution: 0.0125 ppm
- Total range: ± 60 ppm
- Goal: minimize error $e_{A,B} = \frac{\alpha_A}{\alpha_B} - 1$
- Implementation: Two-level linear proportional controller



¹Analog Devices, AD9364 Reference Manual, 2014, rev.0.

- Under the assumption that
 - α_A/α_B approx. linear during measurement
 - Relative movement in between satellites is negligible in comparison to frequency difference, or known elsehow
- ... α_A/α_B can be estimated from the phase difference by

$$\frac{\alpha_A}{\alpha_B} = \frac{\Delta\varphi}{2\pi f_c (\hat{\tau}_{B,RX,N+1} - \hat{\tau}_{B,RX,N})} + 1.$$

Carrier Phase Offset

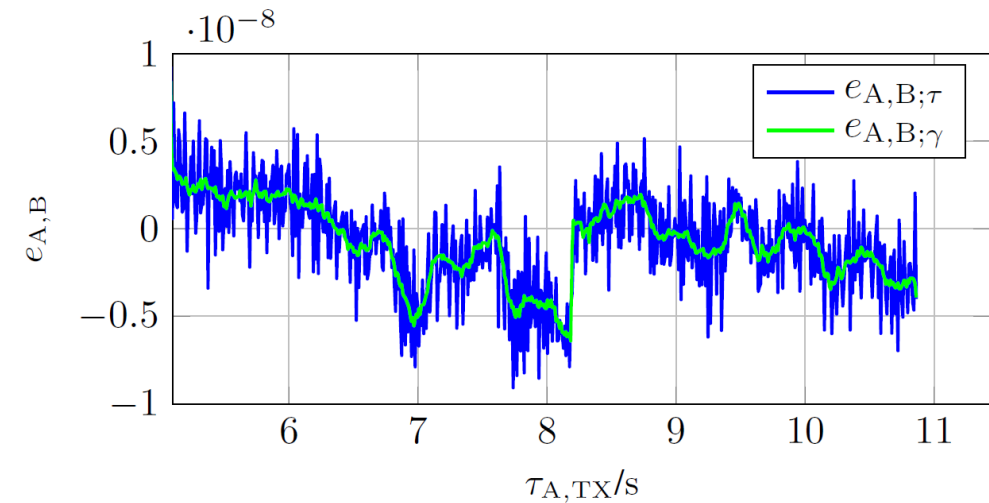
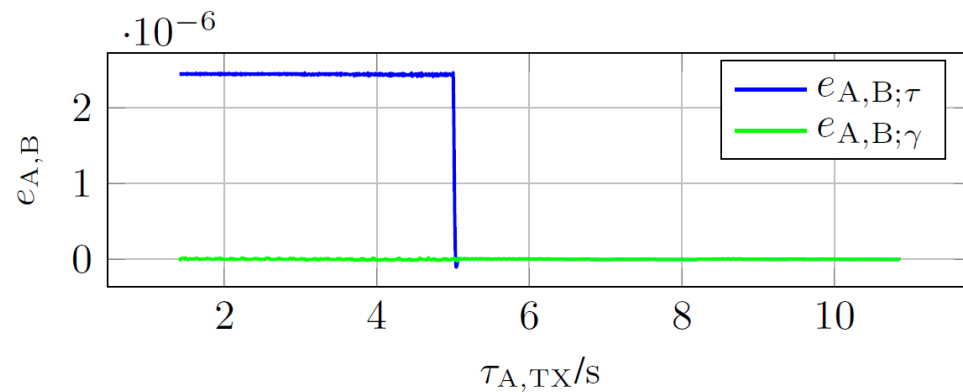
- Considering that $f_{\text{err}} = \left(\frac{\alpha_i}{\alpha_j} - 1 \right) f_c$,
- and using a transformation $t_{i,\text{RX},\text{N}} = 0$ (TWTT measurement starts at 0 global time)

- the relative carrier phase difference is

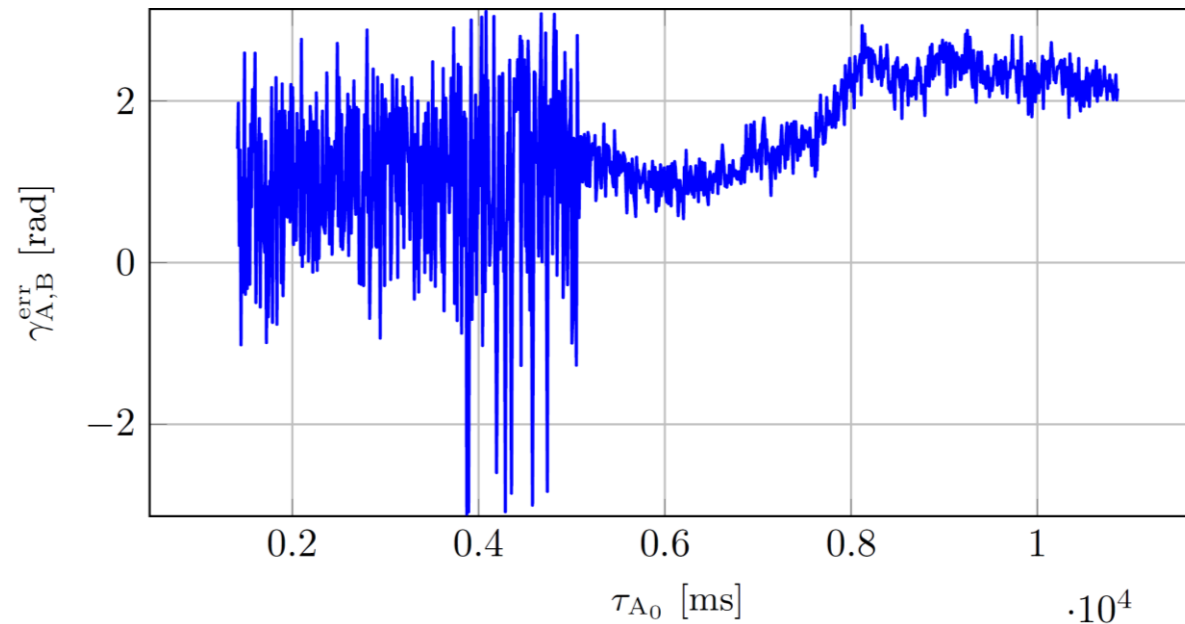
$$\gamma_{i,j}^{\text{err}} = \angle d_{i,j}(\hat{\tau}_{i,j}) - 2\pi f_c \left[\phi_i - \phi_j - \frac{\alpha_i}{\alpha_j} \tau_{j\text{TOF}} - \left(\frac{\alpha_i}{\alpha_j} - 1 \right) (\tau_{j,\text{RX}} - \tau_{j,\text{TX}}) \right].$$

- **Note:** $\Delta T_{i,j} = \phi_j - \phi_i$, α_i/α_j , $\tau_{j\text{TOF}}$, $\tau_{j,\text{RX}}$, $\tau_{j,\text{TX}}$ are known.

- Using two development kits at a distance of approx. 1.8m
- Evaluation using $n_{\text{trial}} = 1000$ TWTT measurements
- Syntonization inactive during first 5 seconds, then frequency matching using DCX0
- $f_c = 2 \text{ GHz}$, $B_c = 34 \text{ MHz}$, $l_c = 1024$ and $f_s = 61.44 \text{ MHz}$
- Settling time $\Delta t = 80 \text{ ms}$



- Settling time possibly caused by PLLs
- Standard deviation $\sigma_{\gamma_{i,j}^{\text{err}}} \cong 0.21 \text{ rad}$ from 289 samples (corresponds to 3.3% of the wavelength)



Summary & Next Steps

- **Summary**
 - Synchronization, ranging and carrier phase offset estimation on commercial CubeSat SDR platform
 - Measurement results show promising performance
- **Next steps**
 - Use measurements for carrier-phase synchronization
 - Make system more robust and extend to more nodes
 - Test under more realistic conditions: ISL link budget, Doppler, free-space, etc.
 - Bring it into a mission!