

WE1H-1

# Direct-Coupled TE-TM Waveguide Cavities

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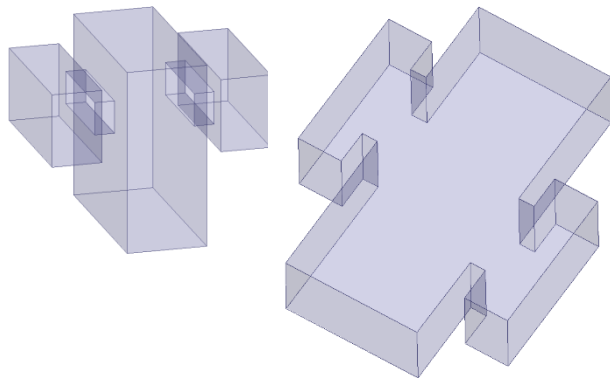
- Introduction
- Direct-Coupled TE-TM Waveguide Cavities
- Coupling Control
- Experimental Result
- Conclusions

# Introduction

**WAVEGUIDE TECHNOLOGY = LOW LOSS + POWER – SIZE**

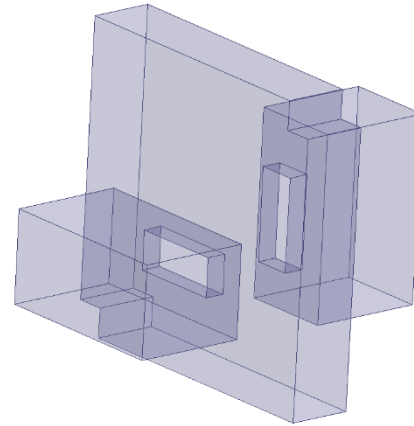
**Cavity structures with enhanced capabilities (multiple poles and/or transmission zeros)**

## TM & TE Singlets



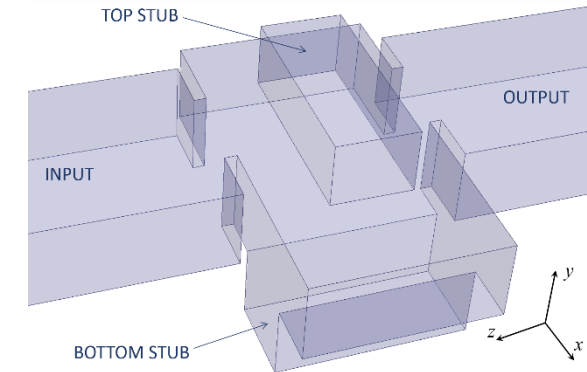
**1 Pole + 1 Zero**

## TM Dual-Mode (Doublet)



**2 Poles + 2 Zeros**

## Stubbed WG Cavity

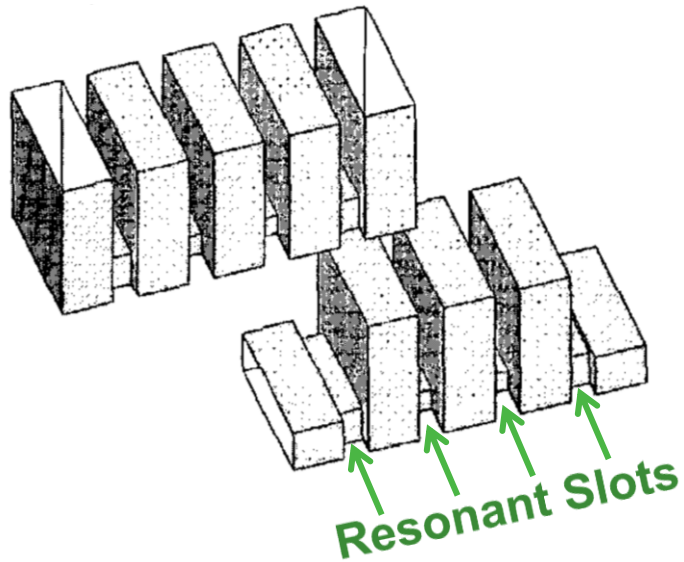


**3 Poles + 2 Zeros**

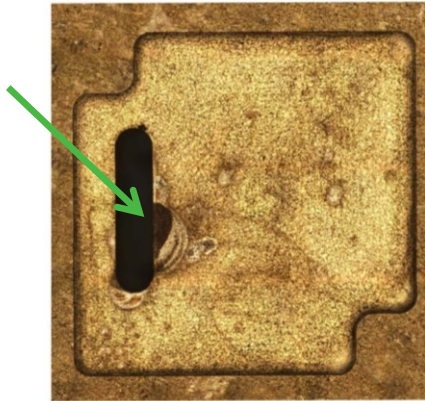
**SUITABLE FOR (AND LIMITED TO) NARROWBAND APPLICATIONS**

For TM pseudo-elliptic filters, wide bandwidths can be obtained by mixing resonant cavities and resonant coupling slots/irises

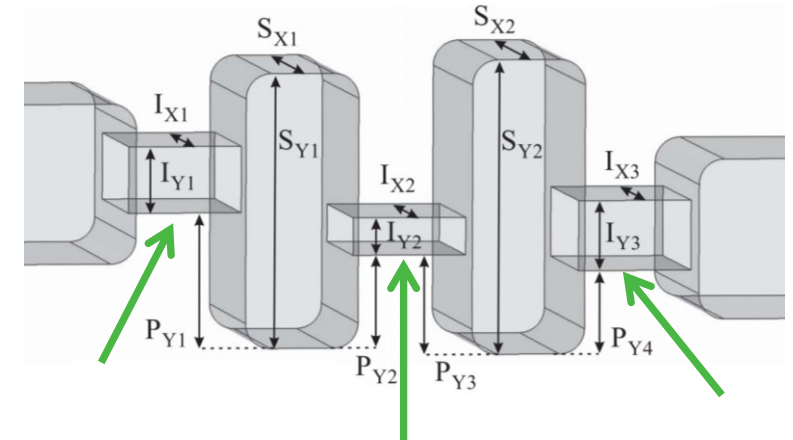
## Pseudo-highpass Filters



## TM Dual-Mode Bandpass



## TM Single-Mode Bandpass



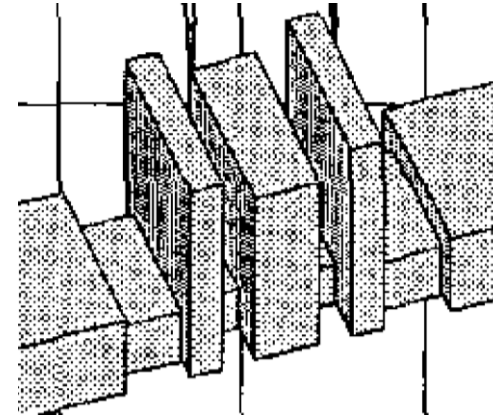
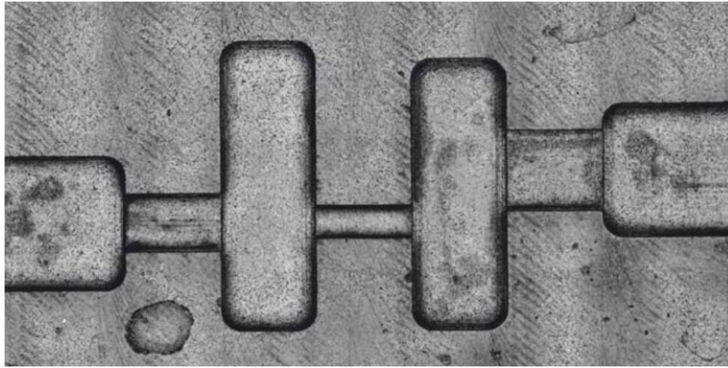
1. U. Rosenberg, *et al.*, "Compact pseudo-highpass filters formed by cavity and iris resonators," *34th European Microwave Conf.*, 2004.
2. C. Bartlett, *et al.*, "Improved TM Dual-Mode Filters With Reduced Fabrication Complexity," in *IEEE Journal of Microwaves*, 2022.
3. C. Bartlett, *et al.*, "Highly Selective Broadband mm-Wave Diplexer Design," in *IEEE Microw. and Wireless Components Letters*, 2022.

# Introduction

Those structures provides brilliant solutions for the purposes they are intended for, but some drawback/limitation has to be considered:

**The heights of the slots (and sometimes the thicknesses)  
are optimization parameters for certain couplings**

**→ *reduced heights are commonly required (low  $Q$ -factor and low power handling)***



**GENERALLY SUITABLE ONLY FOR WIDEBAND PSEUDO-ELLIPTIC RESPONSES**



# Introduction

## OBJECTIVE OF THIS WORK:

**TO FIND A MORE GENERAL CONFIGURATION THAT IS CAPABLE OF REALIZING BOTH NARROW AND WIDE BAND RESPONSES, THUS PAVING THE WAY FOR THE INTRODUCTION OF A NEW CLASS OF DIRECT-COUPLED WAVEGUIDE FILTERS POSSESSING**

- 1) THE STRENGTHS OF THE MOST ADVANCED TM PSEUDO-ELLIPTIC FILTERS, AND**
- 2) AND THE DESIGN VERSATILITY (BANDWIDTH) OF THE MOST CONVENTIONAL IRIS-COUPLED CAVITY FILTERS**

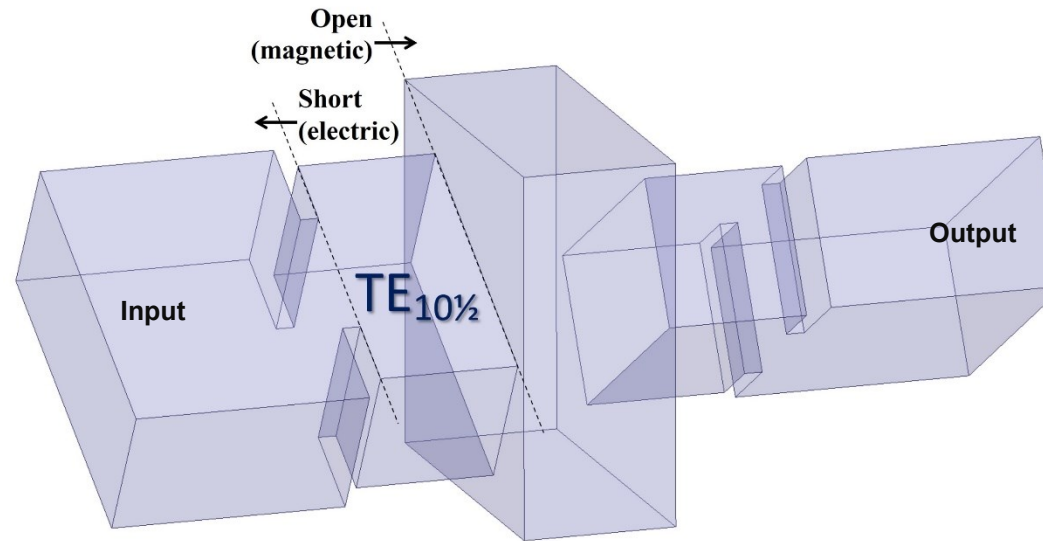
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# Direct-Coupled TE-TM Cavities

**BASIC IDEA:** TE<sub>10</sub> sections and TM<sub>11</sub> section are directly coupled without any dedicated coupling discontinuity between them

The rectangular TE sections are directly terminated into the much larger square TM section  
→ *the equivalent of an open-ended (magnetic) condition is seen at one end of the TE sections*

**Basic TE-TM-TE  
Three-section  
Configuration**



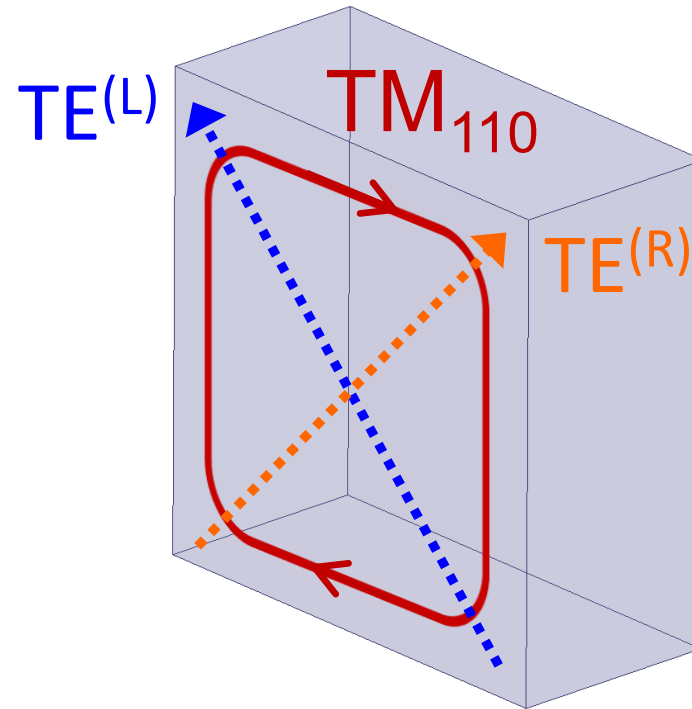
→ TE half-mode resonating with a quarter-wavelength variation along the longitudinal direction becomes feasible within each TE section



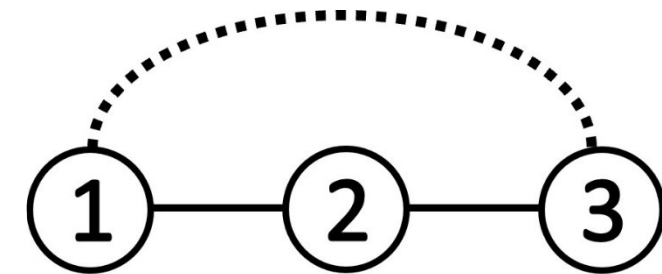
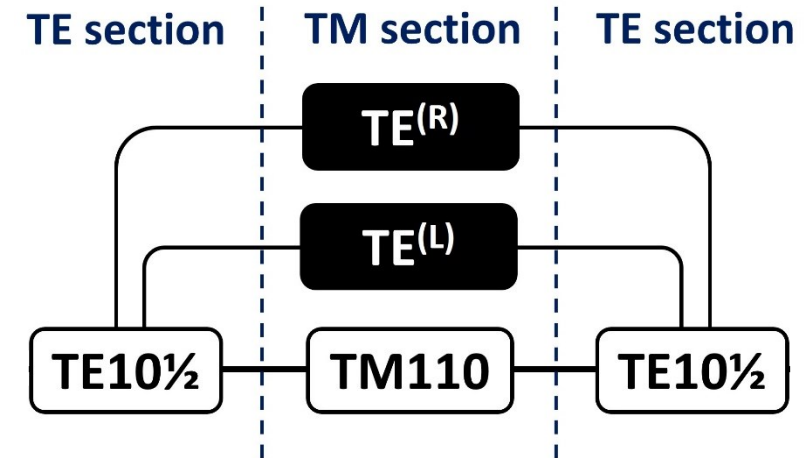
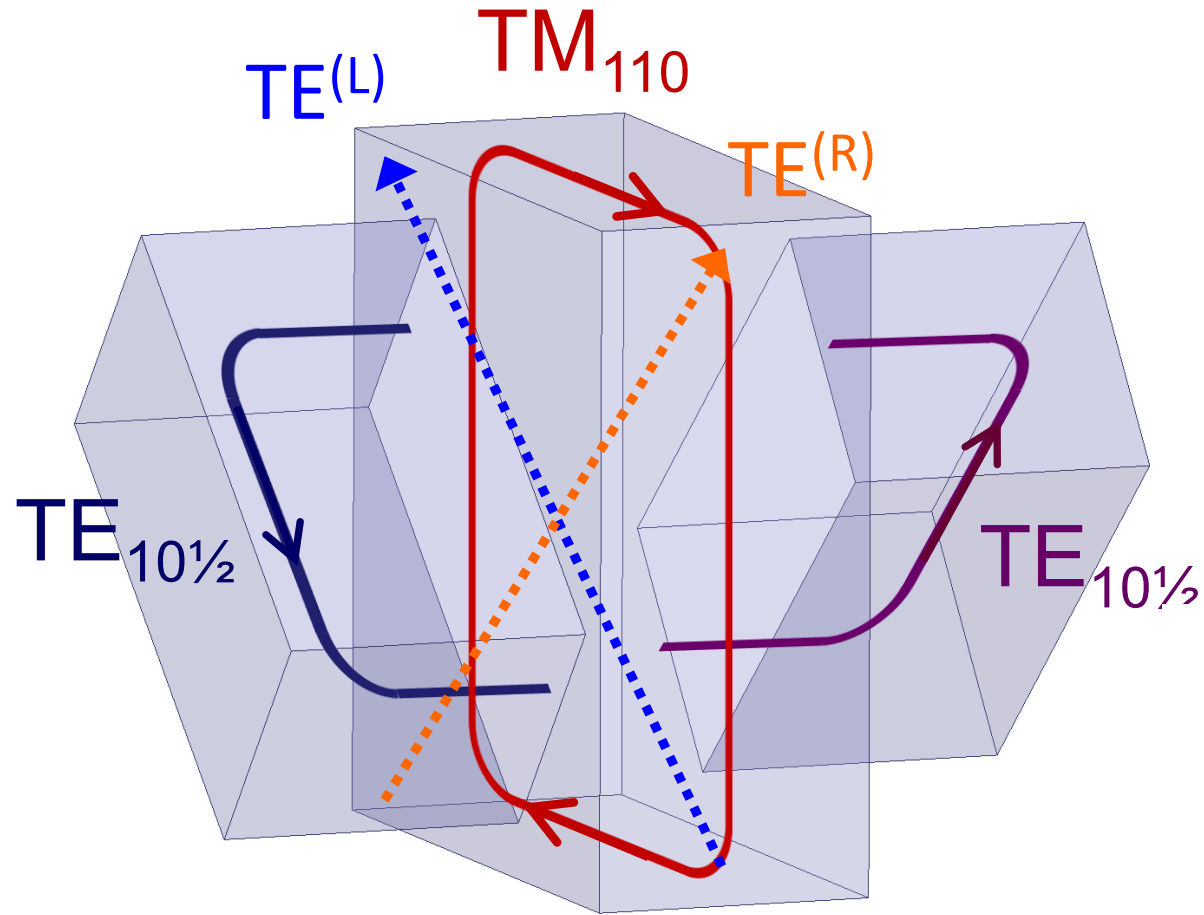
# Direct-Coupled TE-TM Cavities

The square cross-section of the TM section is sized to support a resonant TM<sub>110</sub> mode

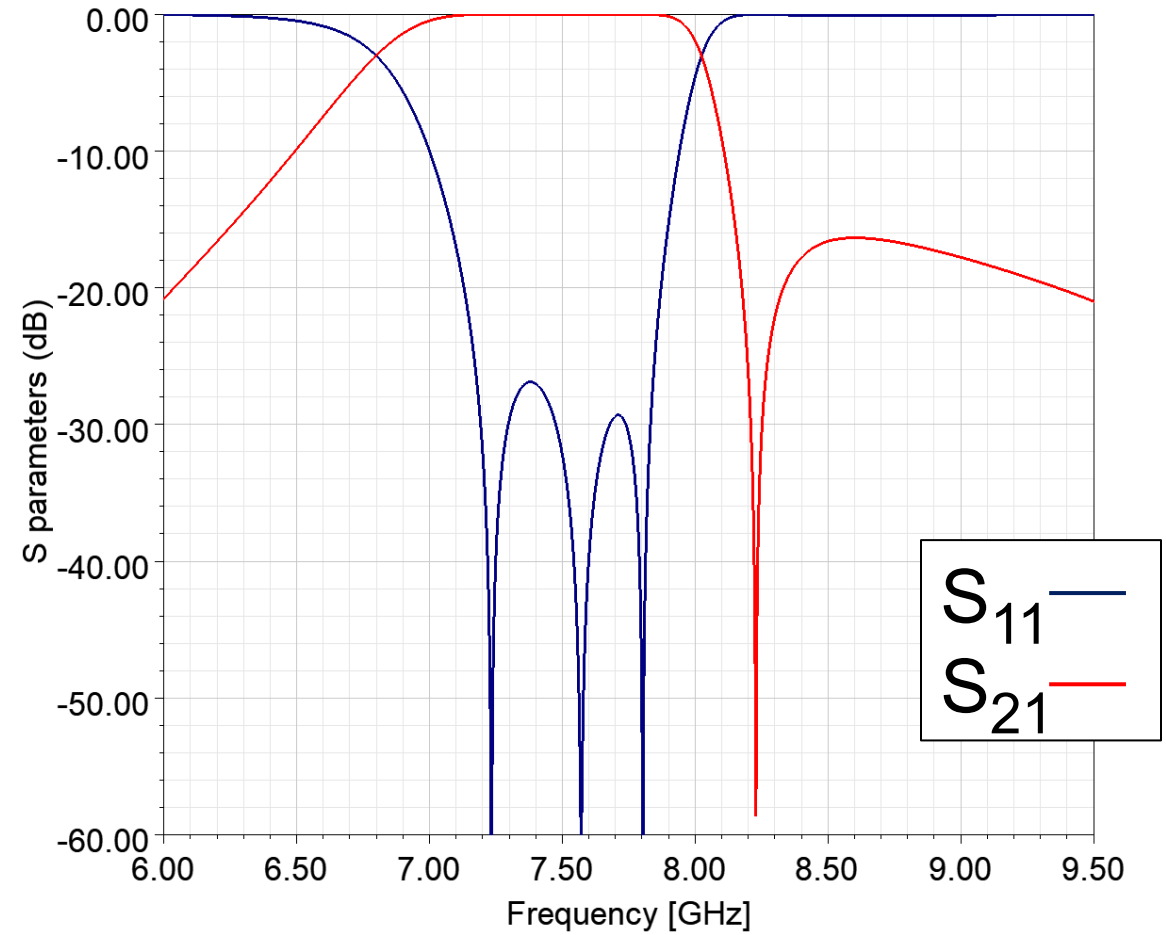
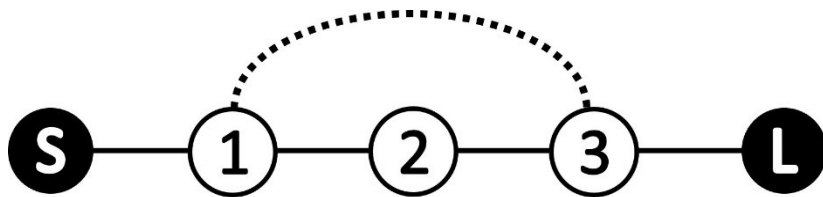
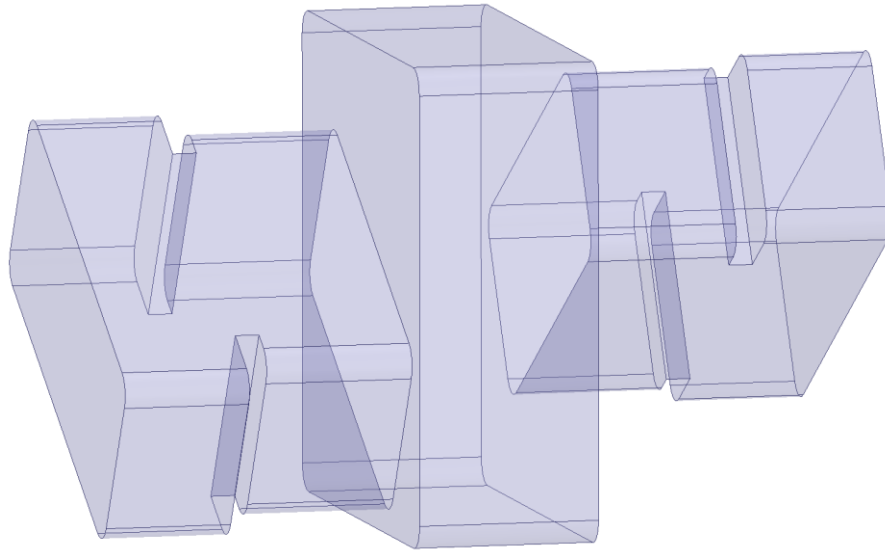
The square TM section also supports a pair of orthogonal nonresonating TE modes, TE(L) and TE(R), which are polarized along its diagonals



# Equivalent Topology



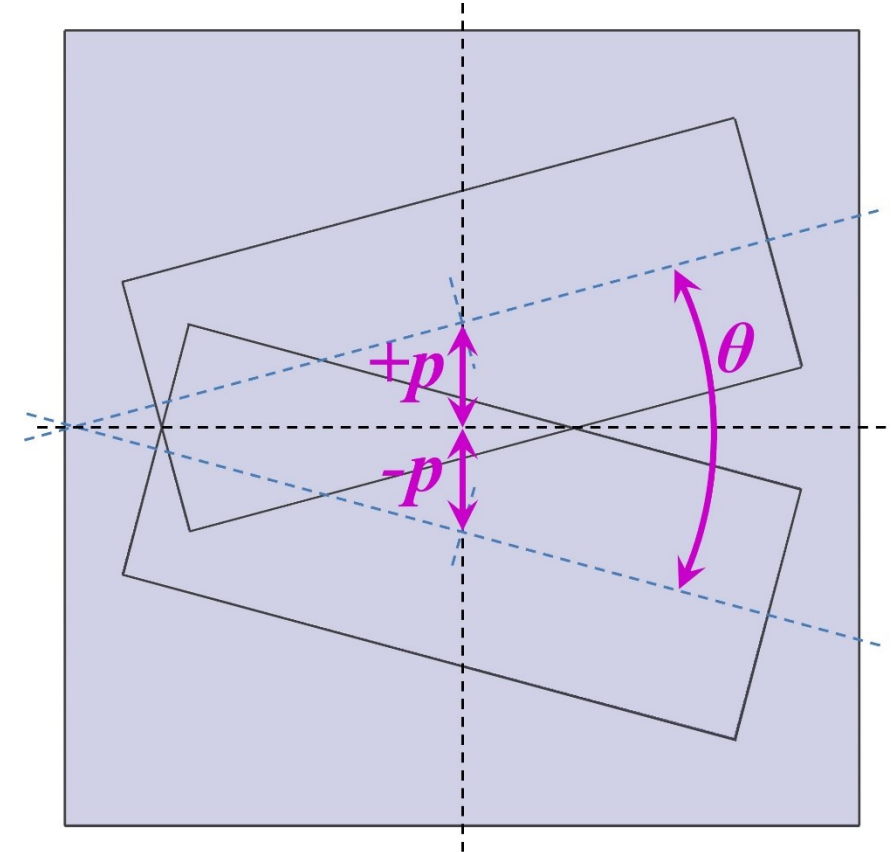
# Typical Response



- Introduction
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**All coupling coefficients are FULLY controlled  
by the POSITION and the ORIENTATION  
of the TE sections**

**The size of the TE sections is NOT employed for  
any coupling purpose  
→ it can be set equal to the full size of a  
standard waveguide  
(maximum unloaded Q-factor)**

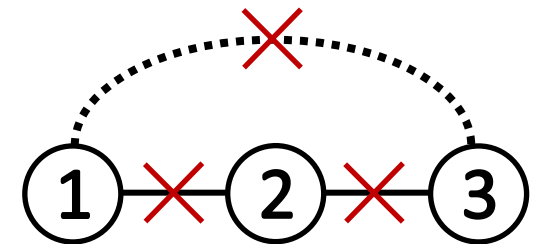
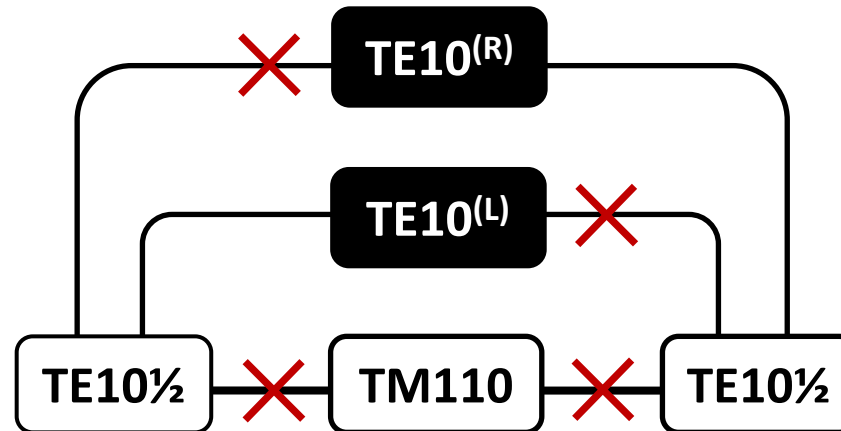
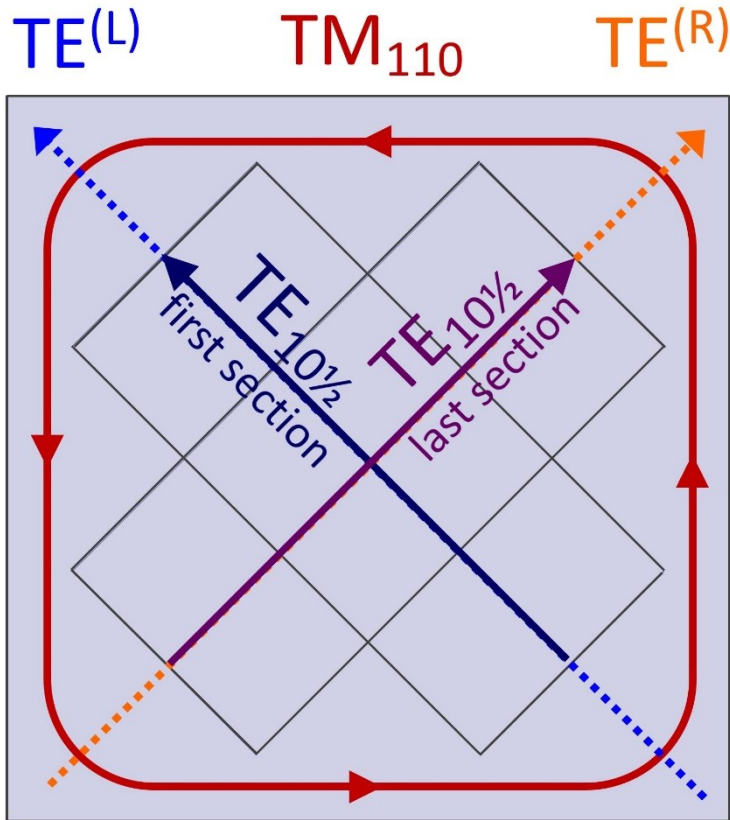




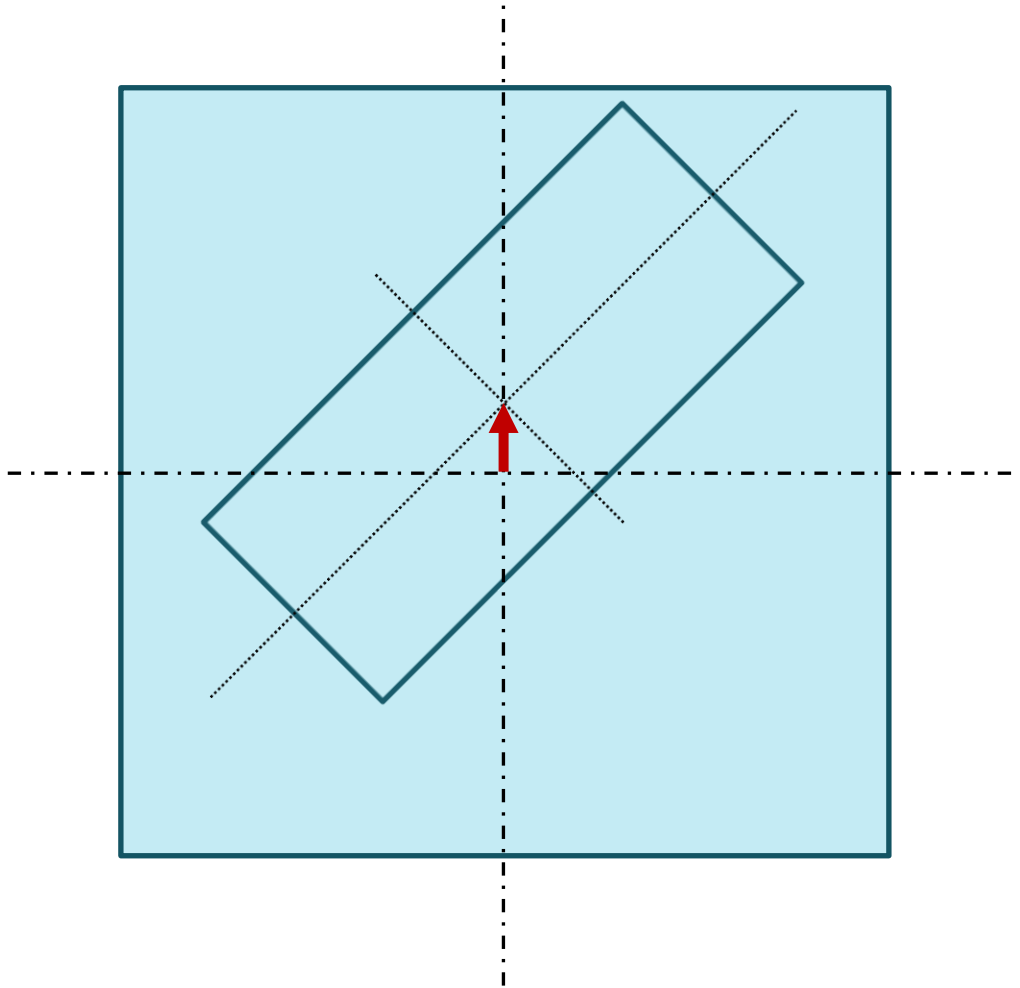
# Total Isolation Condition

- 1) TE sections are centered ( $p=0$ )
- 2) TE sections parallel with diagonals ( $\theta=90^\circ$ )

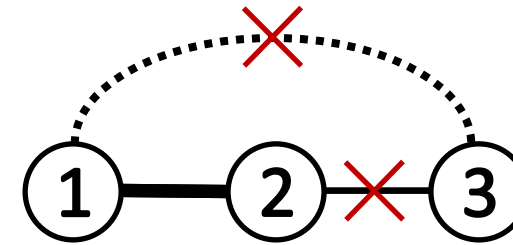
**ALL MODES ARE UNCOUPLED/ISOLATED**  
**→ TM110 mode cannot be excited and no by-pass coupling between TE modes can occur**



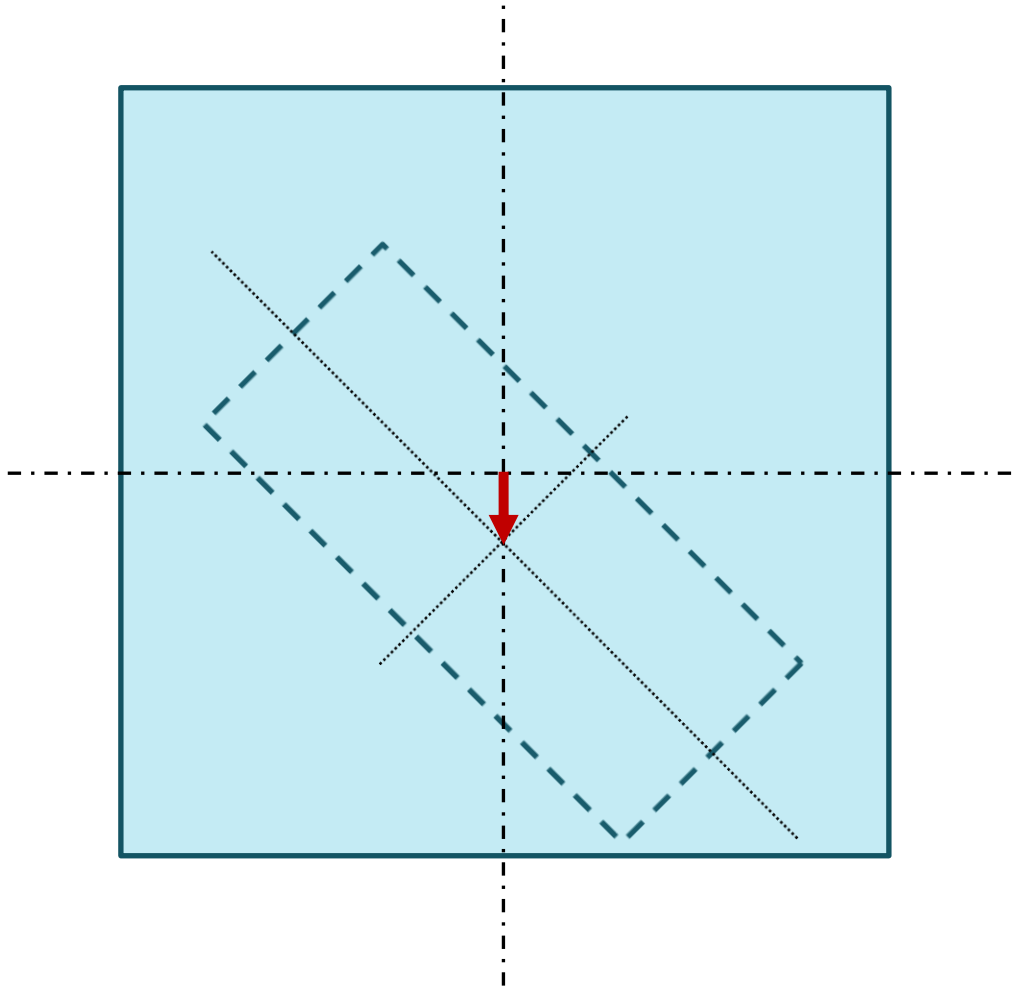
# Coupling Control



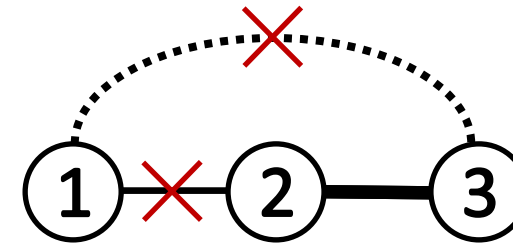
Starting from the isolation condition:  
the offset of the first TE section  
controls the coupling between its  
TE<sub>10</sub> and the TM<sub>11</sub>  
→ Coupling M<sub>12</sub>



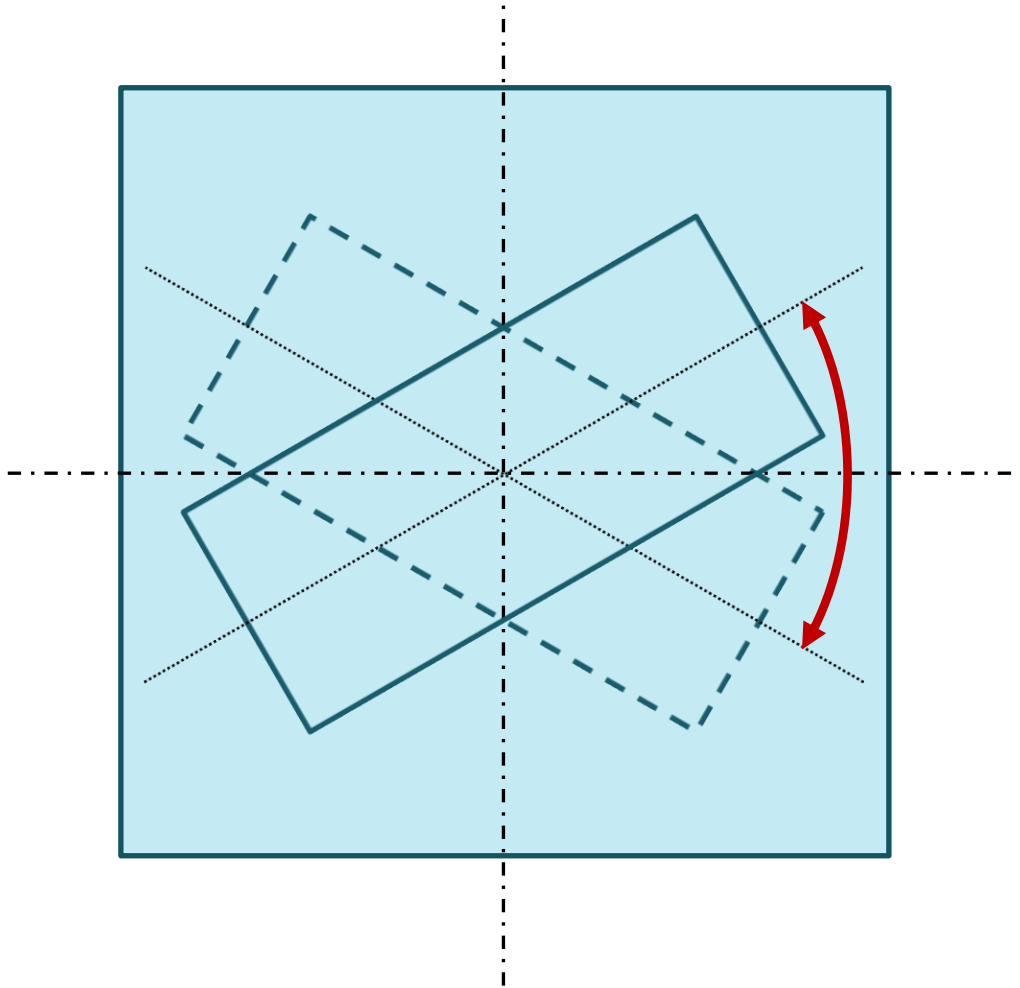
# Coupling Control



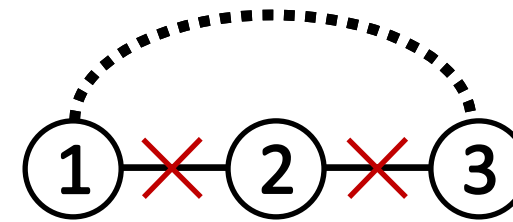
Starting from the isolation condition:  
the offset of the third TE section  
controls the coupling between its  
TE<sub>10</sub> and the TM<sub>110</sub>  
→ Coupling M<sub>23</sub>



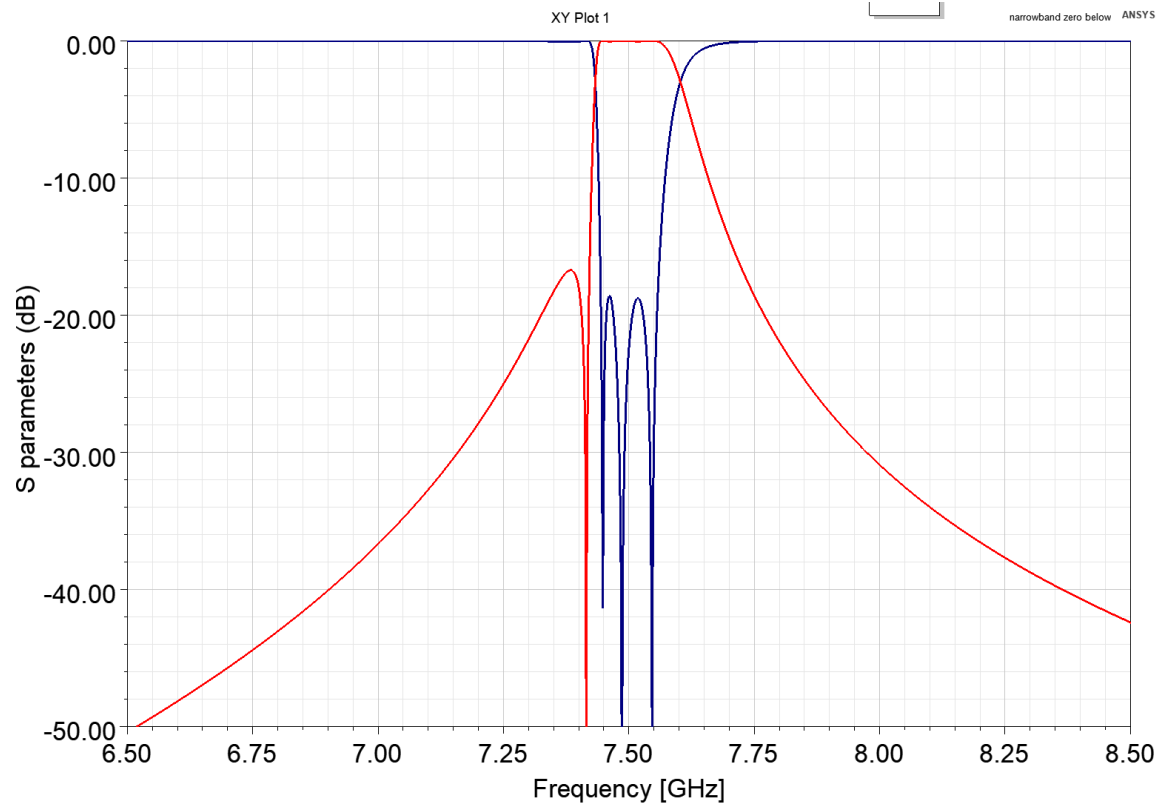
# Coupling Control



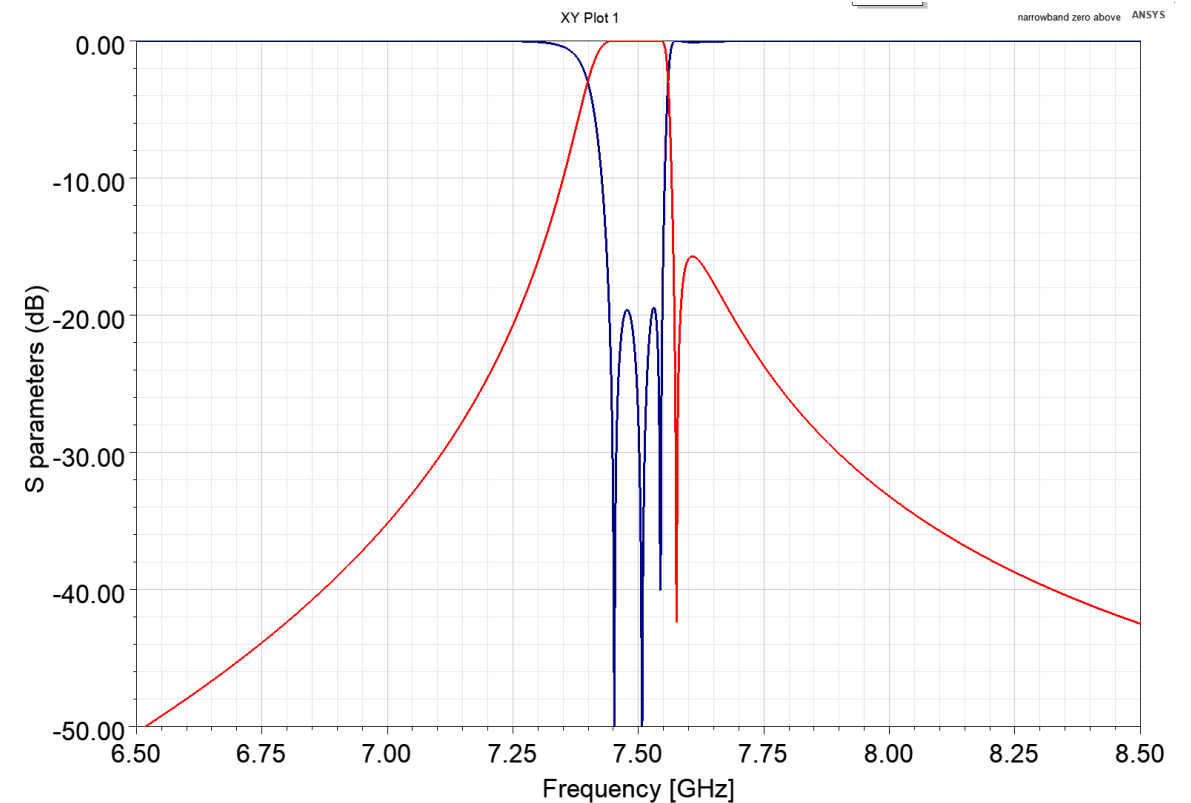
Starting from the isolation condition:  
the angle between the TE sections  
controls the by-pass coupling between  
the two TE $10\frac{1}{2}$  modes  
→ Coupling M13



## TE sections offset SAME directions

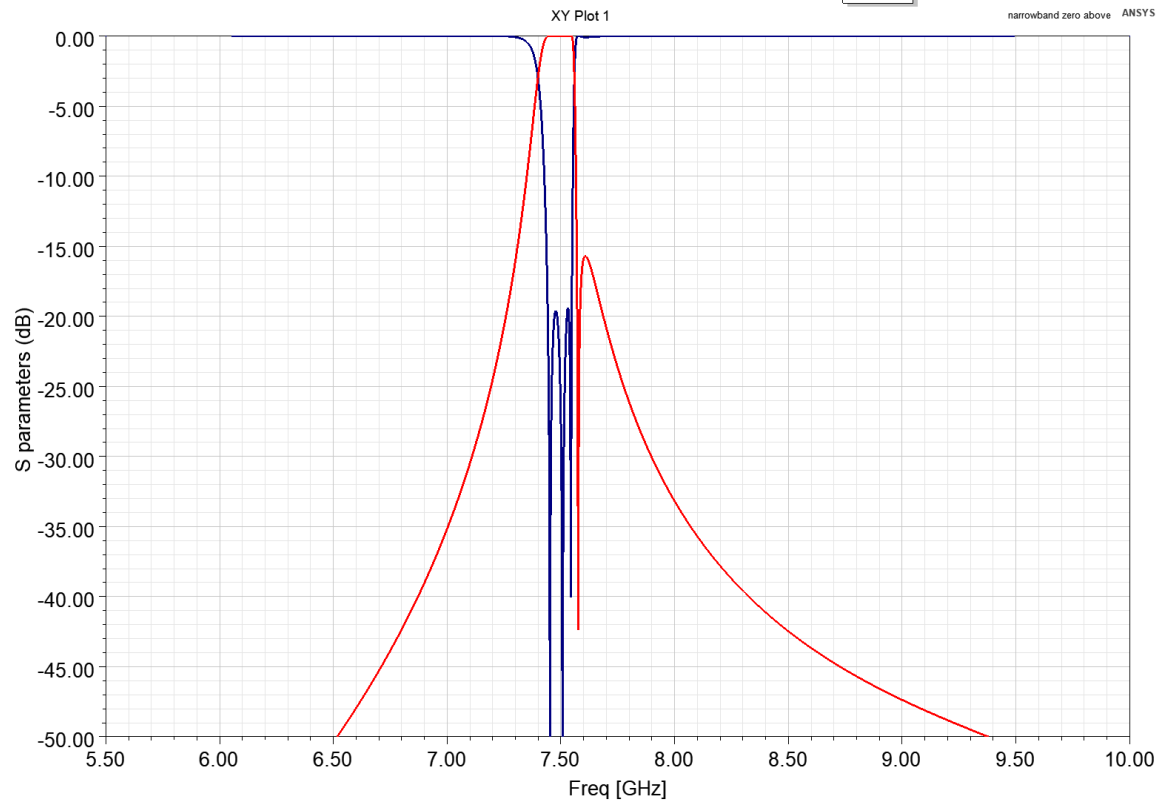


## TE sections offset OPPOSITE sides

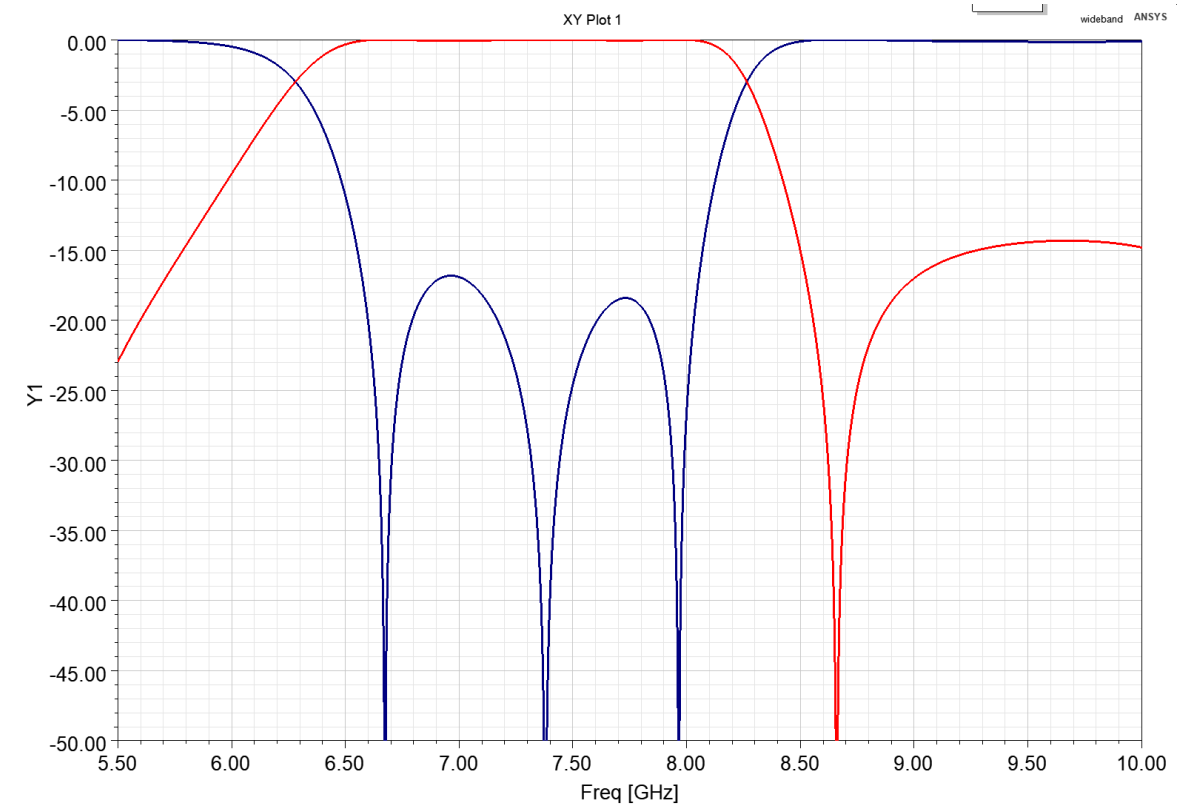




## Small Offsets + Almost Right Angle

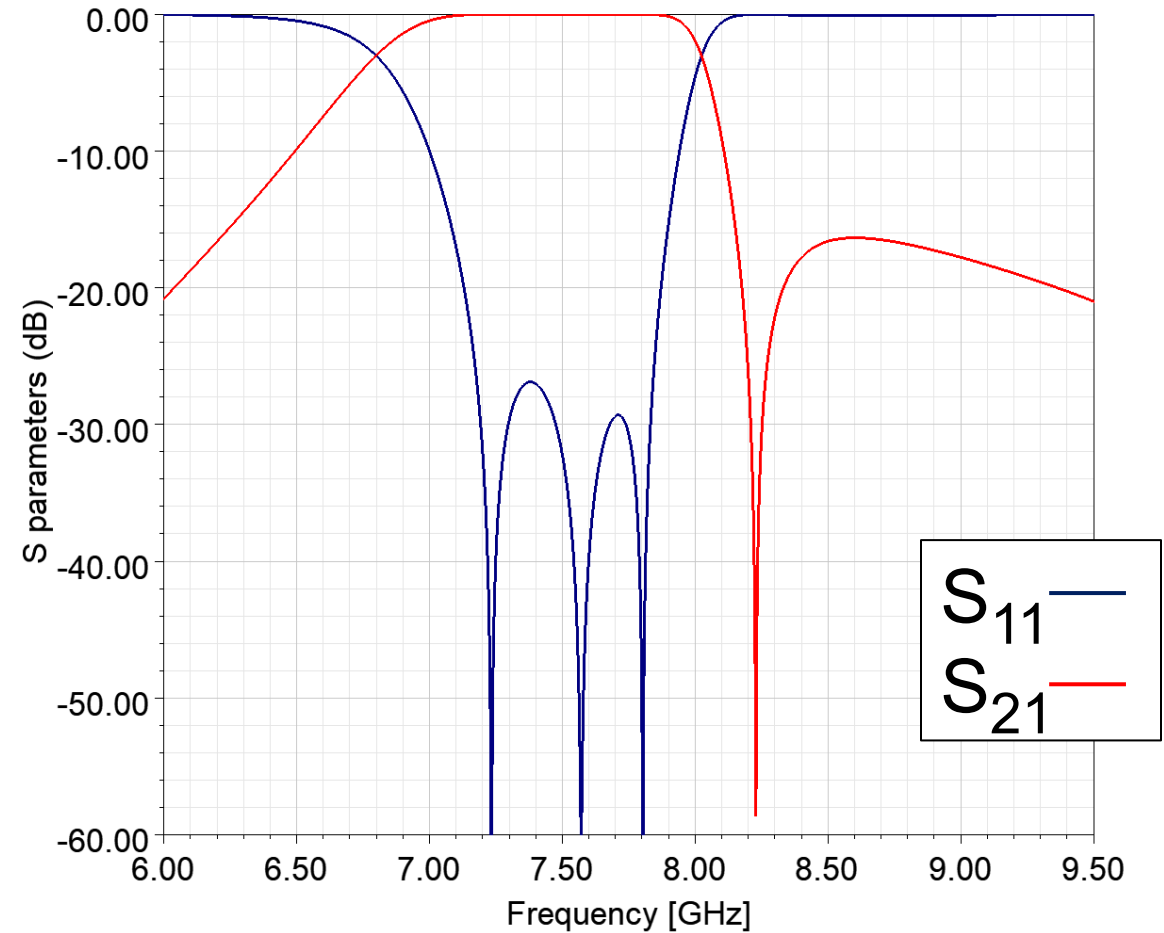
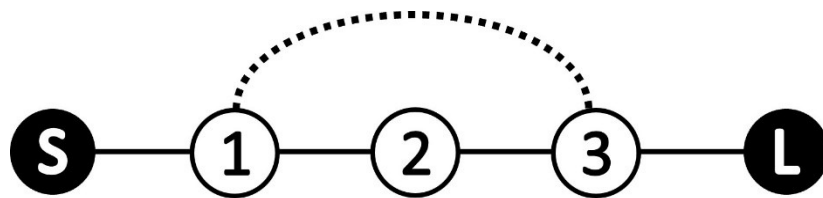
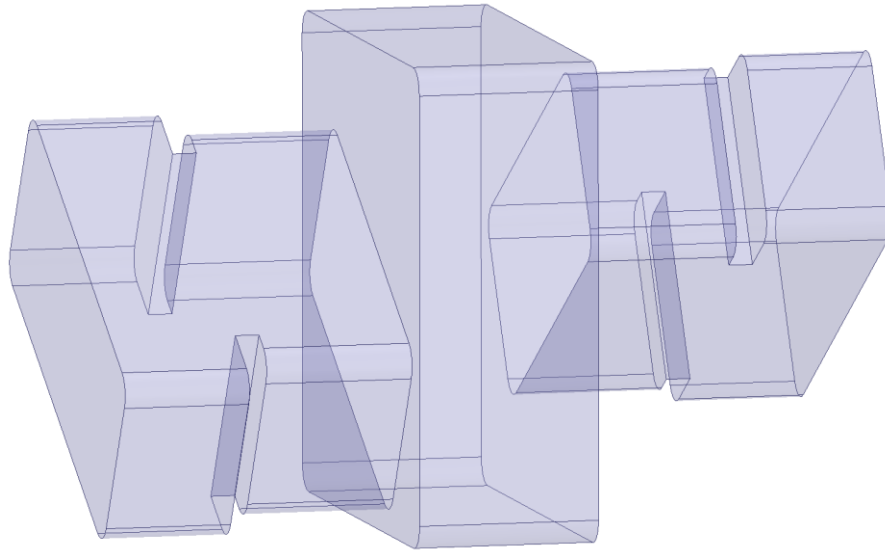


## Large Offsets + More Acute Angle

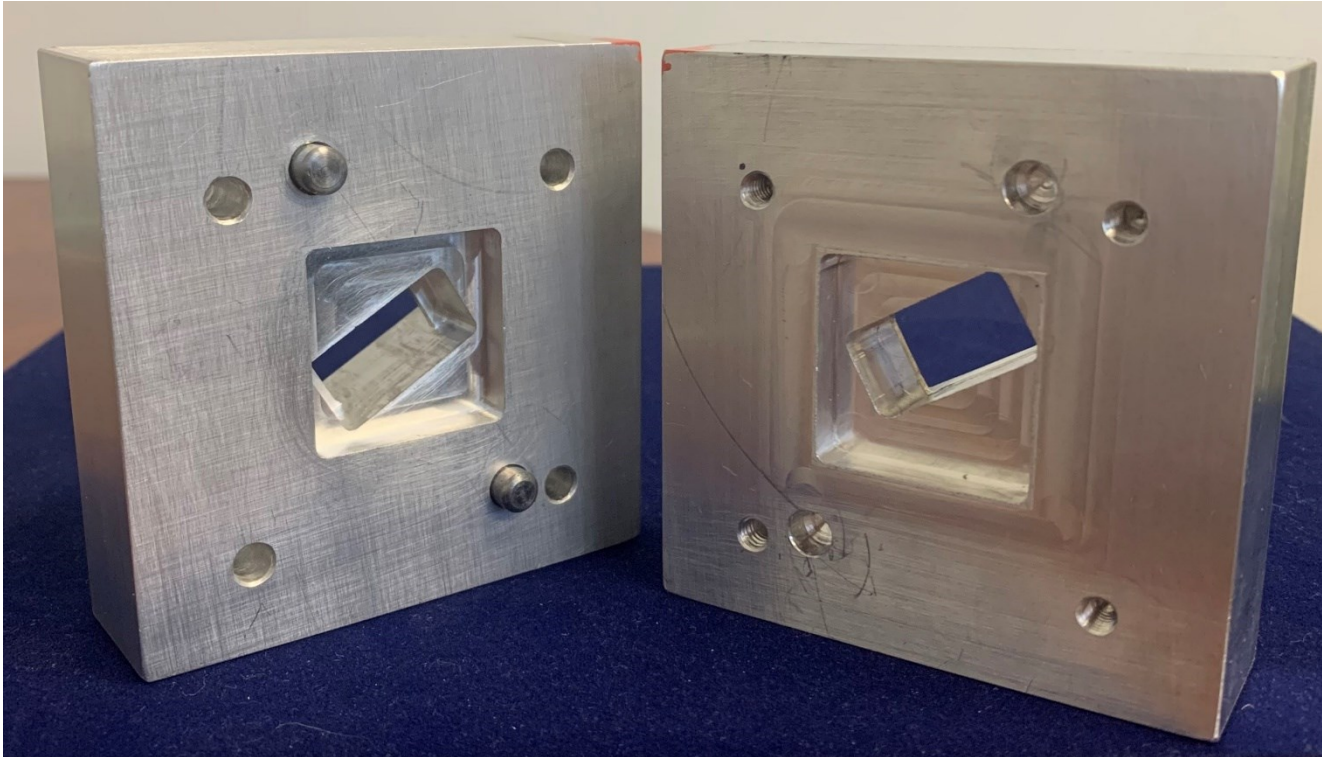


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# Basic TE-TM-TE Configuration

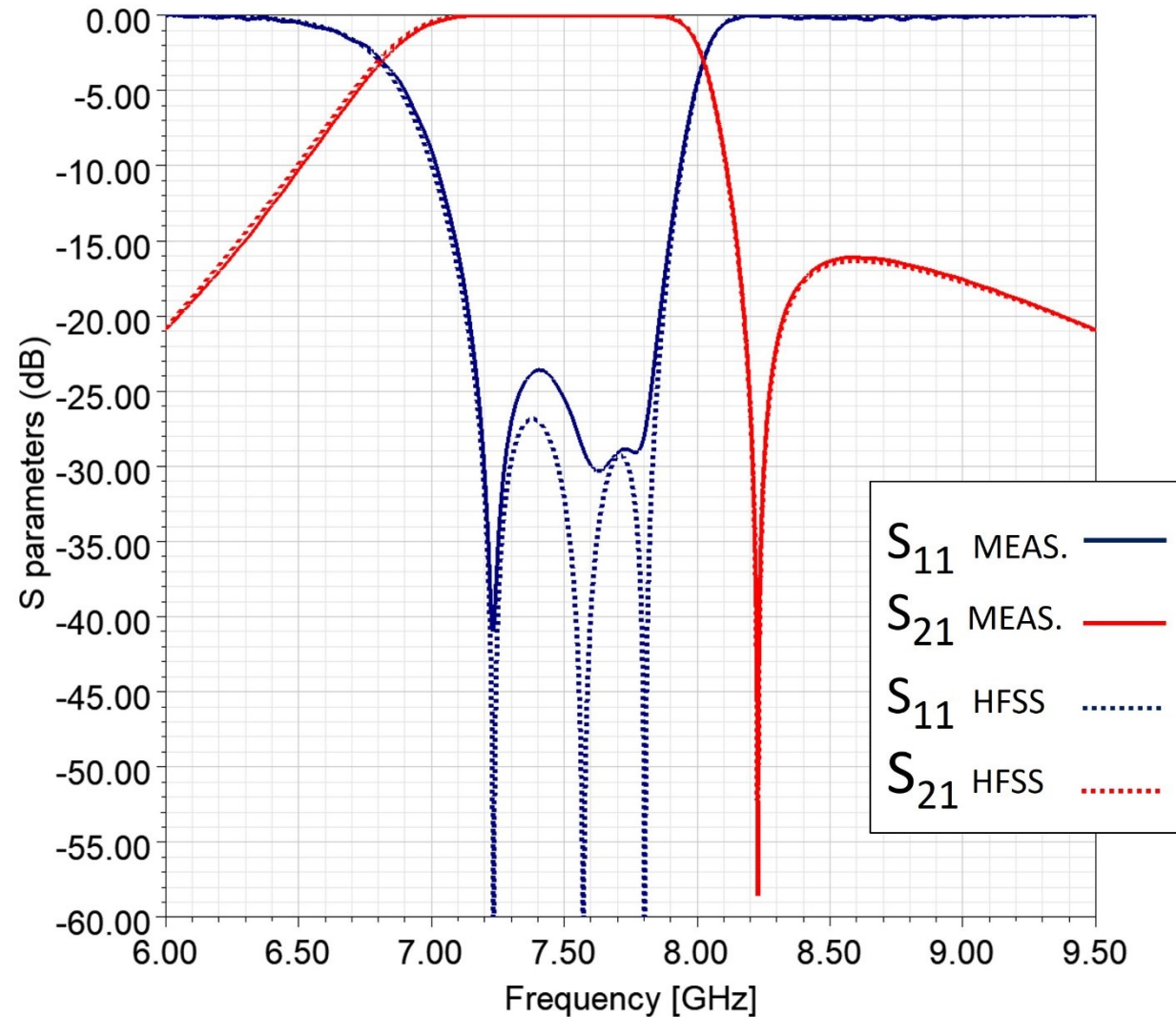


# Manufactured Prototype



**Aluminum prototype  
(no silver plating)**

**→ WR112 flanges are  
manufactured on the other  
side of each block**

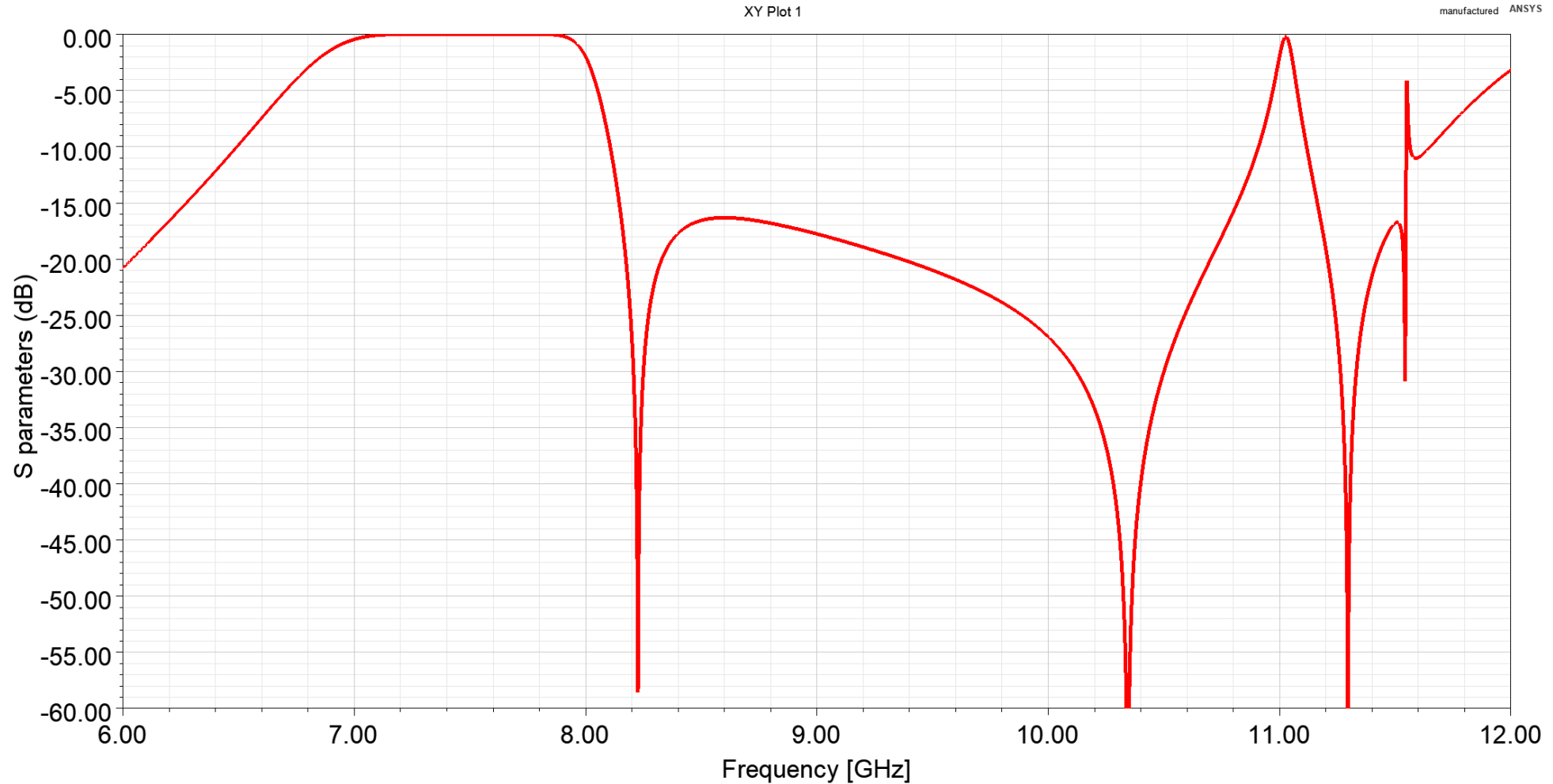


**Insertion loss < 0.05 dB**  
**Average Experimental Q≈5600**

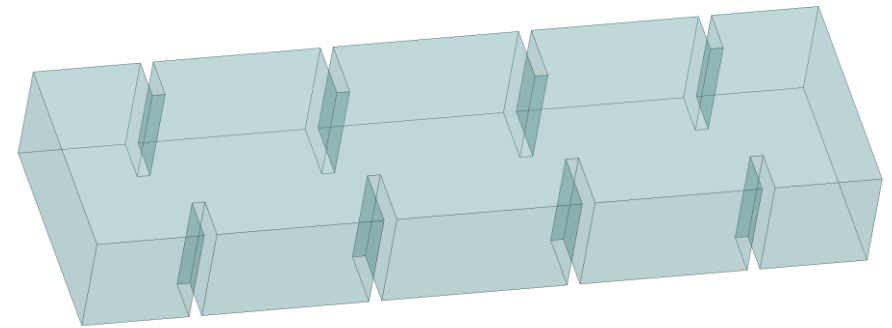
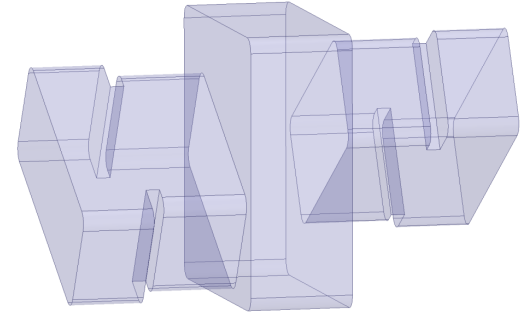
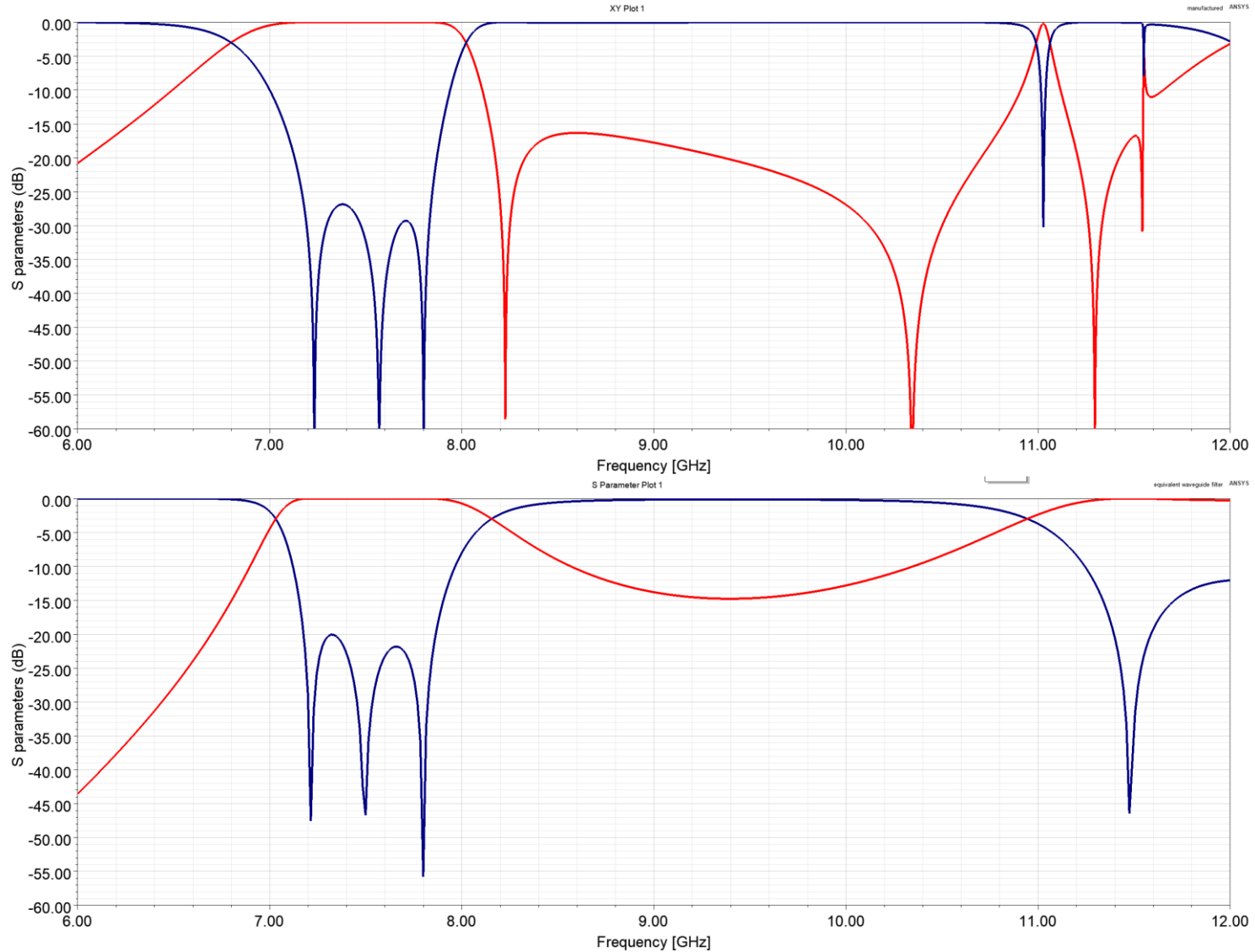
→ the simulated unloaded Q  
for ideal silver surfaces are  
**8000 for the TE<sub>10</sub> and**  
**9300 for the TM<sub>11</sub>**



# Spurious Free Stopband



# Comparison vs Standard WG



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# Conclusions

- Innovative structure based on direct-coupled TE-TM sections (with no dedicated coupling element)
- Basic building block for the definition of a new class of direct-coupled waveguide filter combining the strengths of the most advanced TM filters and the versatility of the more standard iris-coupled waveguide filters
- Future development: higher order filters

# ...Thank You...

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