

#### **We3G-5**



# X-Parameters: The µ Stability Factor and Its Application to Avoid Oscillation Problems During the Characterization of Power GaN FETs

E.A. Hernández-Domínguez<sup>1</sup>, **J.R. Loo-Yau**<sup>1</sup>, A. Sánchez-Ramos<sup>1</sup>, J.A. Reynoso-Hernández<sup>2</sup>, P. Moreno<sup>1</sup>



<sup>1</sup>Centro de Investigación y Estudios Avanzados del I.P.N. Unidad Guadalajara, Zapopan, Jalisco, México



<sup>2</sup>Centro de Investigación Científica y de Educación Superior de Ensenada, Ensenada, Baja California, México





#### Outline

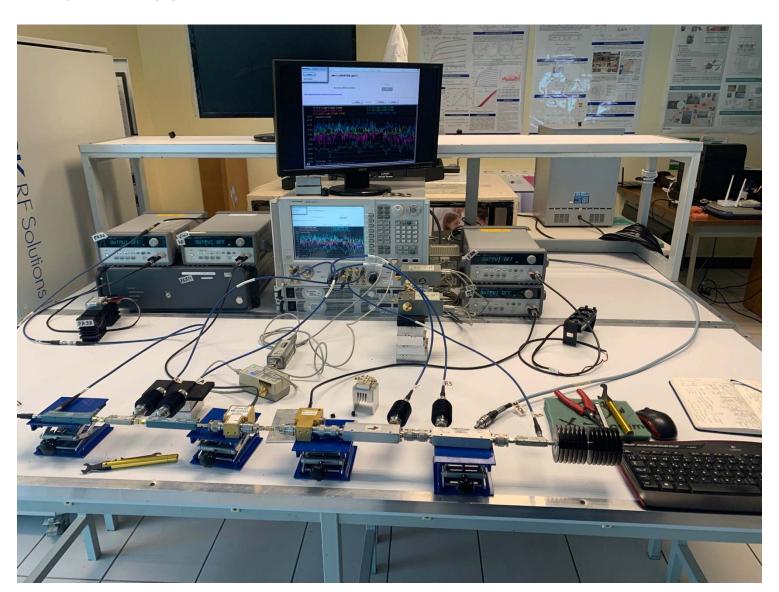


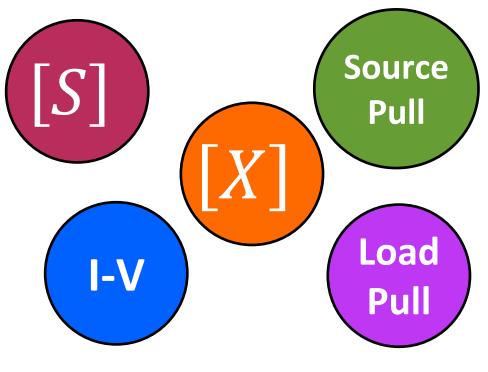
- 1. Introduction
- 2. X-Parameters Background
- 3. The  $\mu$  Stability Factor in Terms of the X-Parameters
- 4. Experimental Results
- 5. Conclusion











Transistor characterization is fundamental for developing:

- Linear Model
- Nonlinear Model
- **■** Microwave Circuits







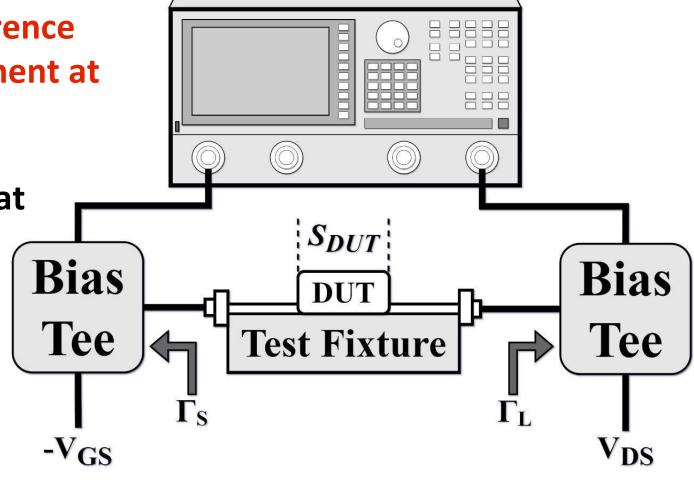


The main concern for many is establishing the reference plane of the measurement at the DUT plane

However, there are other things that

one should worry about

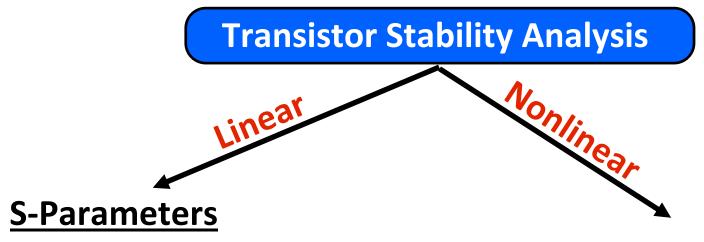
An instability problem could appear, making it impossible to characterize the FET







Instability during the characterization process is something that is not mentioned very often



- Rollet Factor (K)
- Stability Circles
- Edward-Sinsky Factor ( $\mu$ )
- Simple methodology 7 Frequency domain
- Easy and straightforward results interpretation

- Nyquist
- Hopf Bifurcation
- Mathematically more complex
- Not easy to interpret the results
- Time&Frequency domain









A simple methodology to analyze the stability of the FET as a function of the frequency and the input power could help to answer the following questions:

- What causes the instability?
- How important is it to analyze the stability of a FET when it is operating in saturation?
- How can we stabilize the FET?





#### Outline



- 1. Introduction
- 2. X-Parameters Background
- 3. The  $\mu$  Stability Factor in Terms of the X-Parameters
- 4. Experimental Results
- 5. Conclusion





# X-Parameters Background



# The X-parameters describe the reflected wave of a Device Under Test (DUT) as a function of the bias (DC) and the input signal as:

$$B_{pk}\left(DC, \left|A_{11}\right|\right) = X_{pk}^{F}\left(DC, \left|A_{11}\right|\right)P^{k} + \sum_{\substack{q=1,l=1\\(q,l)\neq(1,1)}}^{q=1,l=1} \left[X_{pkql}^{S} a_{ql} P^{k-l} + X_{pkql}^{T} a_{ql}^{*} P^{k+l}\right]$$
(1)

The harmonic of the output voltage

Describe the change in the traveling wave between the ports p and q at the hamonics k and l

#### Where:

**p** the output port

*q* the inputport

l harmonic of the input port



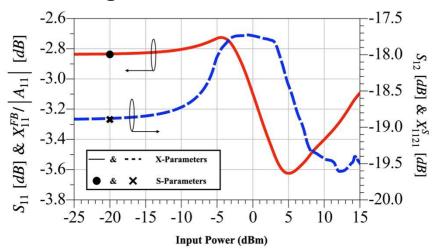


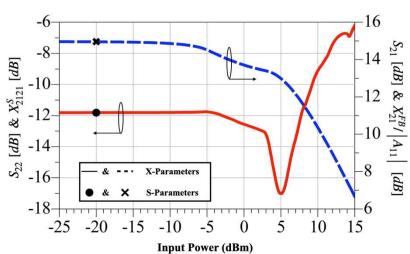


# X-Parameters Background



# At low input power the X<sup>S</sup> term converge with the S-Parameters

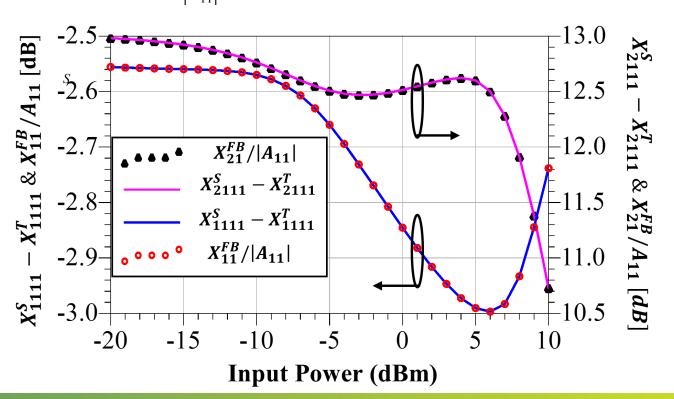




#### Whereas the Large-Signal (LS) behavior can be described by:

$$S_{11}^{LS} \to X_{1111}^{ST} = \frac{X_{11}^F}{|A_{11}|}$$
 (2a)  $S_{12}^{LS} \to X_{1121}^{ST} = X_{1121}^S - X_{1121}^T P^2$  (2b)

$$S_{21}^{LS} \to X_{2111}^{ST} = \frac{X_{21}^F}{|A_{11}|}$$
 (2c)  $S_{22}^{LS} \to X_{2121}^{ST} = X_{1121}^S - X_{2121}^T P^2$  (2d)







#### Outline



- 1. Introduction
- 2. X-Parameters Background
- 3. The  $\mu$  Stability Factor in Terms of the X-Parameters
- 4. Experimental Results
- 5. Conclusion





# The µ Stability Factor in Terms of X-Parameters



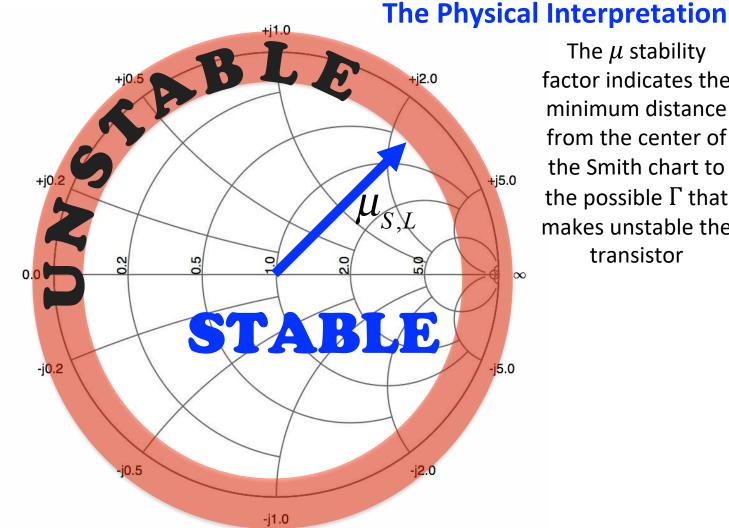
#### The $\mu$ stability factor is defined as:

$$\mu_{S} = \frac{1 - \left| S_{22} \right|^{2}}{\left| S_{11} - \Delta S_{22}^{*} \right| + \left| S_{21} S_{12} \right|}$$
 (3)

$$\mu_{L} = \frac{1 - \left| S_{11} \right|^{2}}{\left| S_{22} - \Delta S_{11}^{*} \right| + \left| S_{21} S_{12} \right|}$$
(4)

Where:

$$\Delta = S_{11}S_{22} - S_{12}S_{21} \tag{5}$$



The  $\mu$  stability factor indicates the minimum distance from the center of the Smith chart to the possible  $\Gamma$  that makes unstable the transistor

If  $\mu_{S,L} > 1$ , the FET is **UNCONDITIONALLY STABLE**, otherwise, the FET is **CONDITIONALLY STABLE** 





# The μ Stability Factor in Terms of X-Parameters



Since S-parameters are for linear regimen,



the question is.... What happened in the nonlinear regimen of the FET?

Thus, the  $\mu$  stability factor in terms of the X-parameters is proposed to write



X-Parameters can describe the nonlinear behavior of the FET

$$\mu_{S}^{ST} = \frac{1 - \left| X_{2121}^{ST} \right|^{2}}{\left| X_{1111}^{ST} - \Delta \left( X_{2121}^{ST} \right)^{*} \right| + \left| X_{2111}^{ST} X_{1121}^{ST} \right|}$$
(6)

$$\mu_L^{ST} = \frac{1 - \left| X_{1111}^{ST} \right|^2}{\left| X_{2121}^{ST} - \Delta \left( X_{1111}^{ST} \right)^* \right| + \left| X_{2111}^{ST} X_{1121}^{ST} \right|}$$
(7)





# The $\mu$ Stability Factor in Terms of X-Parameters



The advantages of using X-parameters in the stability analysis are:

- Allows to analyze the stability of the FET in frequency and input power.
- The interpretation of the stability analysis is straightforward.
- The analysis time is reduced compared with other methods.





#### Outline



- 1. Introduction
- 2. X-Parameters Background
- 3. The  $\mu$  Stability Factor in Terms of the X-Parameters
- 4. Experimental Results
- 5. Conclusion









#### 

X-Parameters

SweepPlan SwpPlan1

Start=2 Stop=4 Step= Lin=101

UseSweepPlan=

SweepPlan=

Reverse=no

X\_Param XP2

Freq[1]=f GHz

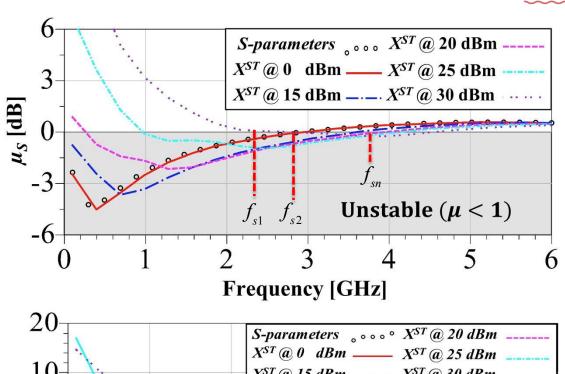
Order[1]=12

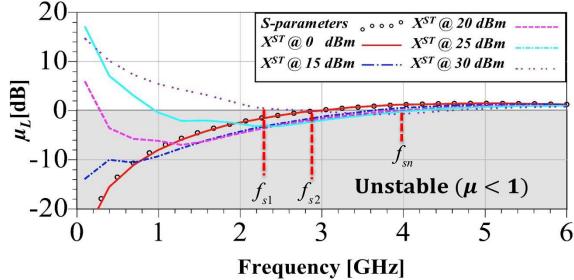
SwpVar[1]="f"

SwpPlan[1]="SwpPlan1"

XParamMaxOrder=3

#### Var Eqn VAR VAR1 f=1.0 X2P XNP2 XP Load XP Source PORT1 PORT2 Num=1 Num=2 Z0=(50+j\*0) Ohm Z0=(50+j\*0) Ohm LS fregHarms[1]=1 Load mode=Impedance LS format[1]=Mag/Phase LS freqHarms[1]=1 LS swpType[1]=Use sweep LS format[1]=Mag/Phase LS value[1,Mag]= LS swpType[1]=Use sweep LS\_start[1,Mag]=dbmtow(-10) LS value[1,Mag]= LS start[1,Phase]=0 LS start[1,Mag]= LS stop[1,Mag]=dbmtow(26) LS stop[1,Mag]= LS stop[1,Phase]= LS numPts[1,Mag]= LS numPts[1,Mag]=37





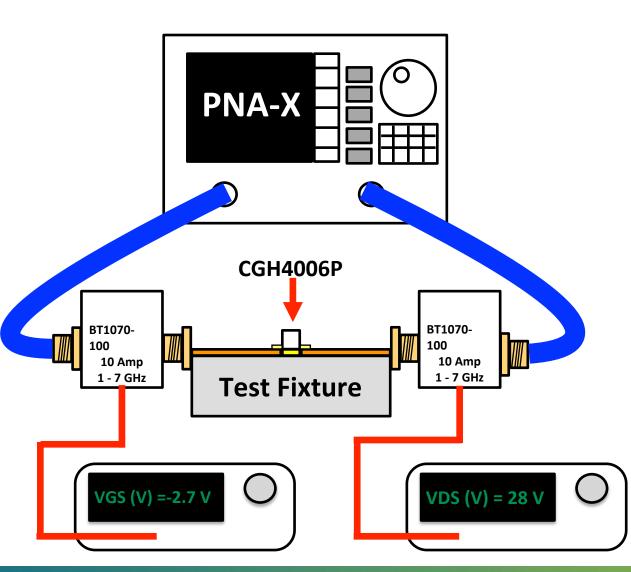


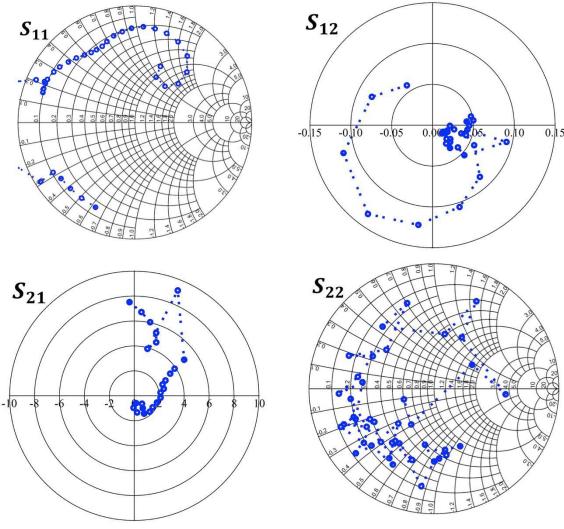


LS numPts[1,Phase]=









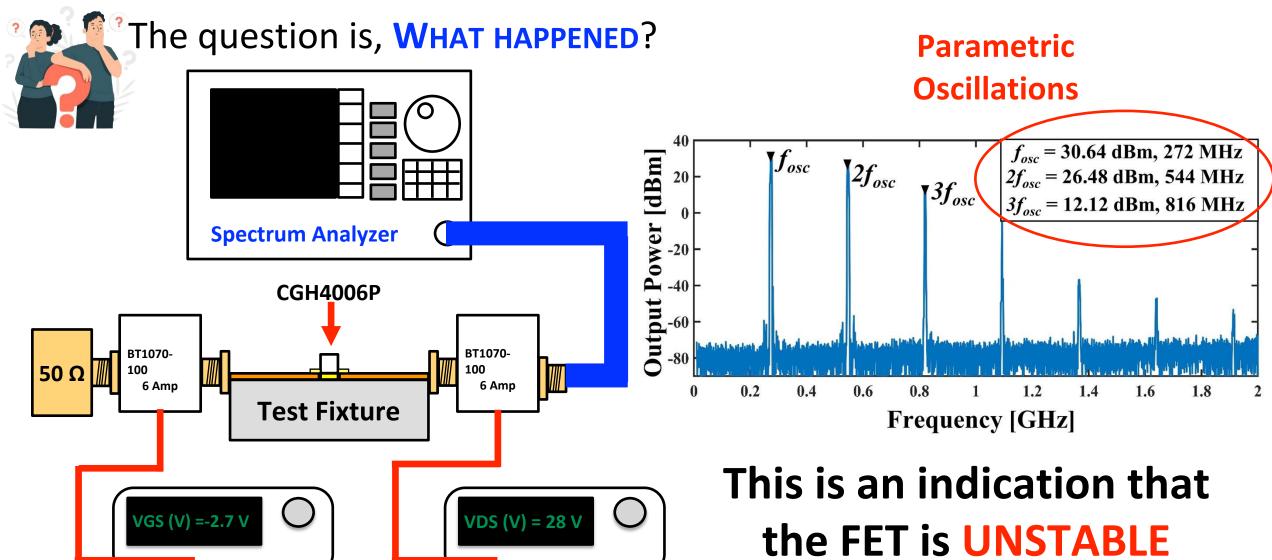
It does not look like a typical S-Parameters measurement







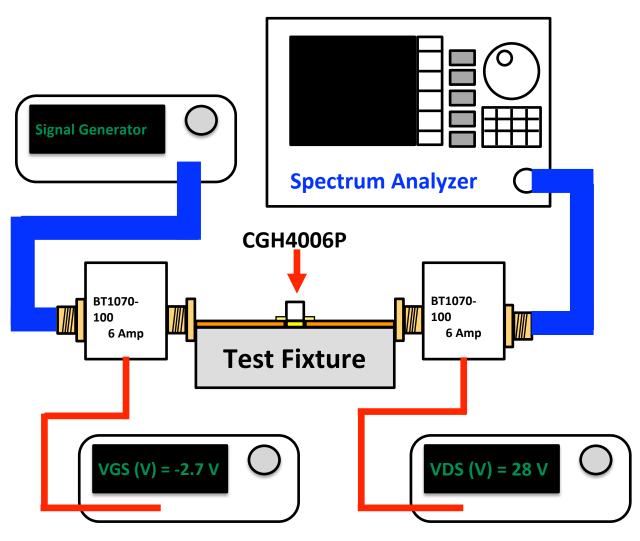




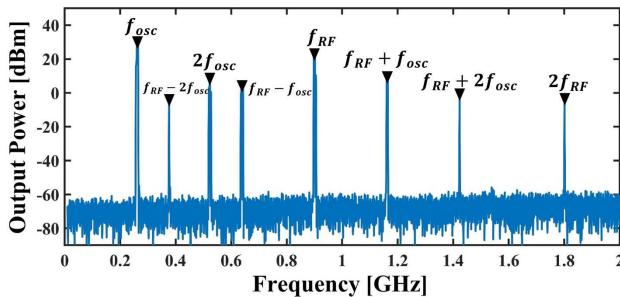










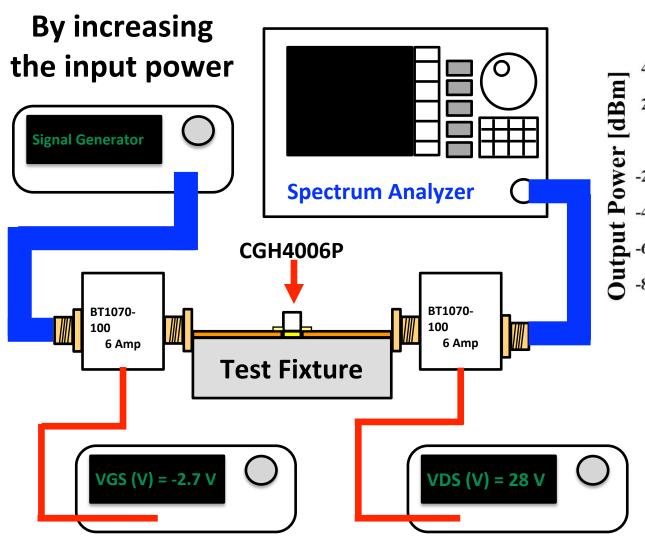


A very **BAD IDEA** to use the FET as an amplifier

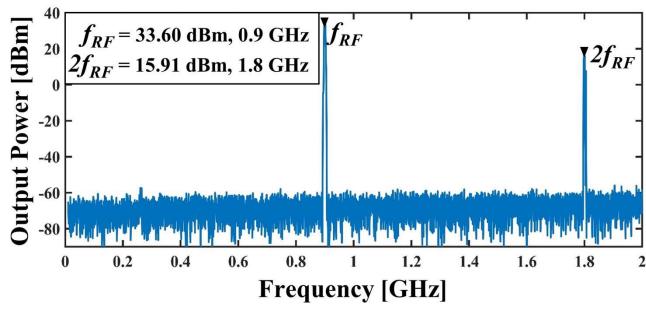








#### ...and as predicted in **SIMULATION**



The parametric oscillations have been disappearing. It seems the FET is **STABLE** 







#### This experiment suggests:

- When the gain is compressed, the FET is stable.
- The main problem of stability lies in the case of low input power.

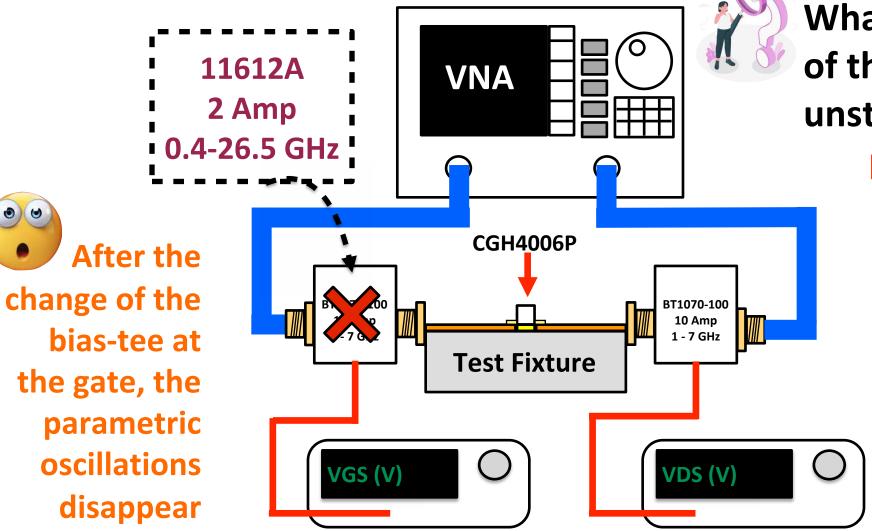


Thus, the classical stability analysis using stability circles could help to understand the instability problem of the FET at the characterization moment









What is the likely cause of the FET being unstable?

Probably the Bias-Tees

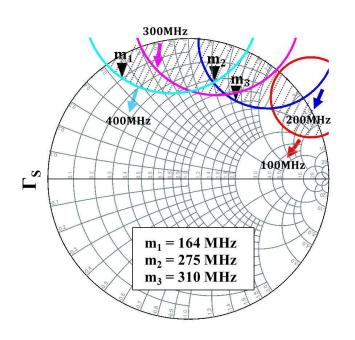
This change corroborates that the bias tees are responsible for the instability

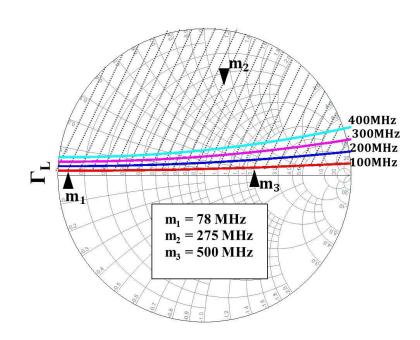






A first approach to verify the effect of the Bias-Tee is computing the input and output stability circle of the FET with the model of the vendor



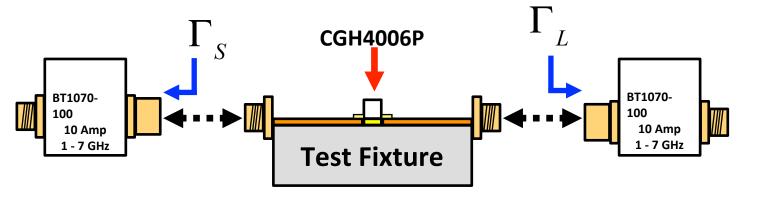


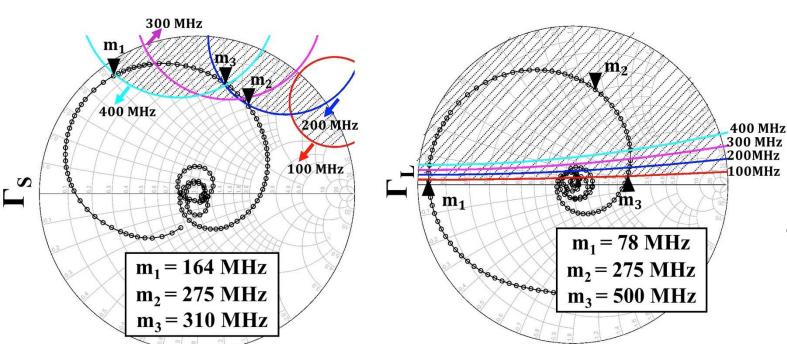
A simulation at low-frequency of the stability circles shows the possible region of  $\Gamma$  can cause the instability of the **GaN FET** 











Comparing the frequency range at which  $\Gamma_{\rm S}$  y  $\Gamma_{\rm L}$  are inside the instability area simultaneously reveals that at 164 – 275 MHz, the FET is potentially unstable

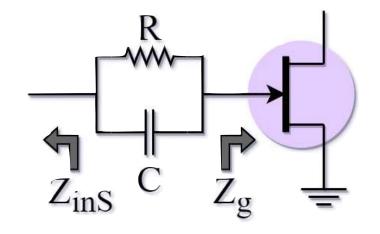
This information is suitable for designing a stability circuit







In the literature, a parallel R-C network in series with the gate of the GaN FET is widely used, but without an explanation of how to determine the value of R or C



This R-C network works as a high-pass filter, where the cut-off frequency ( $f_c$ ) is determined as:

# $f_c = \frac{\kappa}{2\pi C\alpha} \pm \frac{\sqrt{R\kappa - \alpha \left[ \left( R + \rho \right)^2 + \kappa^2 - 8\operatorname{Re}\left( Z_{inS} Z_g \right) \right]}}{2\pi RC\alpha} \tag{4}$

#### Where:

$$\kappa = \operatorname{Im}(Z_{inS} + Z_g) \tag{5}$$

$$\rho = \text{Re}(Z_{inS} + Z_g) \tag{6}$$

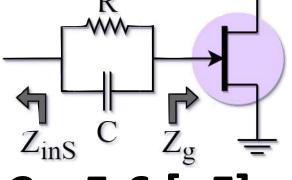
$$\alpha = \kappa^2 + \rho^2 - 8\operatorname{Re}(Z_{inS}Z_g) \quad (7)$$







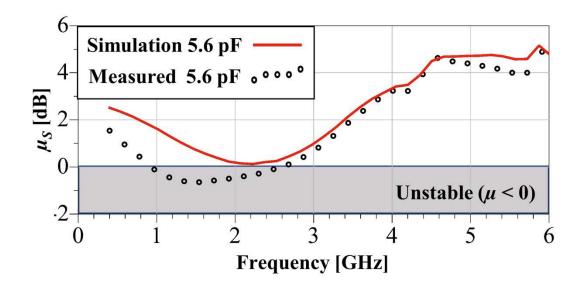
Thus, assuming a  $f_c$  = 0.4 GHz, R = 100  $\Omega$ ,  $Z_{inS}$  = 50  $\Omega$ , and  $Z_g$  is the input impedance of the FET obtained with Sparameters

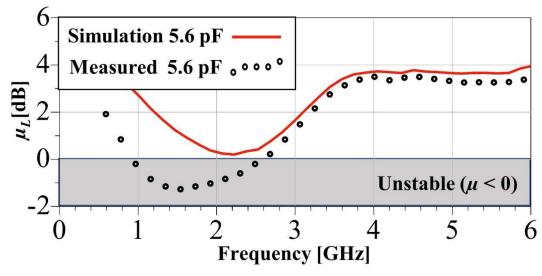


$$C = 5.6 [pF]$$



Simulations do not agree with the measurements, and it seems that it is unstable



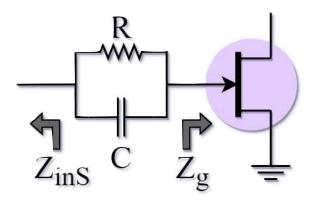






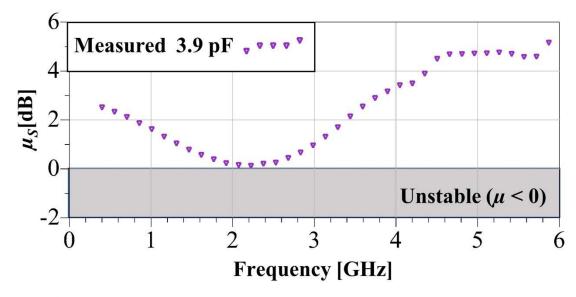


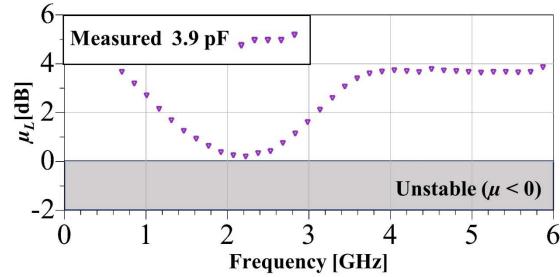
#### Tuning the value of C, shows that



$$C = 3.9 [pF]$$

Now the measurements show that the FET is STABLE



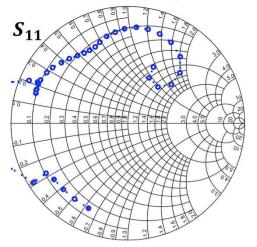


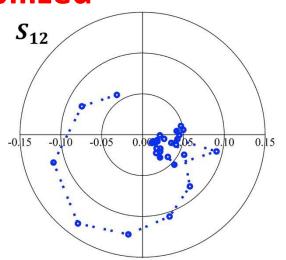


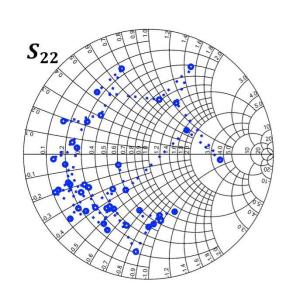




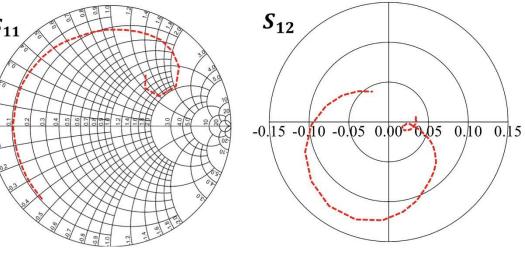
#### w/o Stabilized

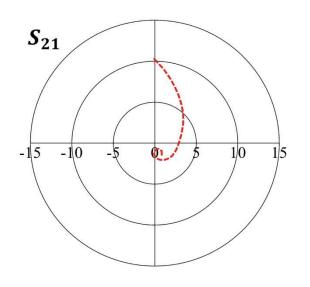


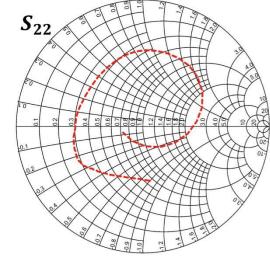




#### **Stable**









 $S_{21}$ 





#### Outline



- 1. Introduction
- 2. X-Parameters Background
- 3. The µ Stability Factor in Terms of the X-Parameters
- 4. Experimental Results
- 5. Conclusion





#### Conclusion



- During the characterization of the FET, the bias tees could be the source that caused the instability.
- Incorporating the X-Parameters in the  $\mu$  factor allows for analyzing the effect of the input power on the stability of the FET.
- The simulation and experimental results corroborated that compressing the gain can stabilize an unstable FET.
- Since the FET under high gain compression level condition is stable, the small-signal stability analysis methods become more relevant.
- Although the results demonstrated that the FET is stable under high-gain compression, it is more recommendable to use a high-pass filter at the gate of FET with cut-off frequency higher than the possible parametric oscillations to stabilize the transistor.

