

We3H/319-NS890

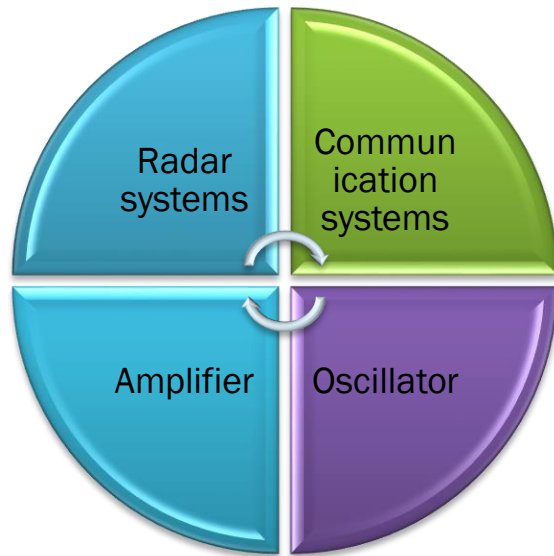
Two-Layer Three-Way Horst Power Divider and Combiner Based-on Microstrip Line with Fixed Characteristic Impedance

A. Zerfaine¹, A. Moulay¹, and T. Djerafi¹

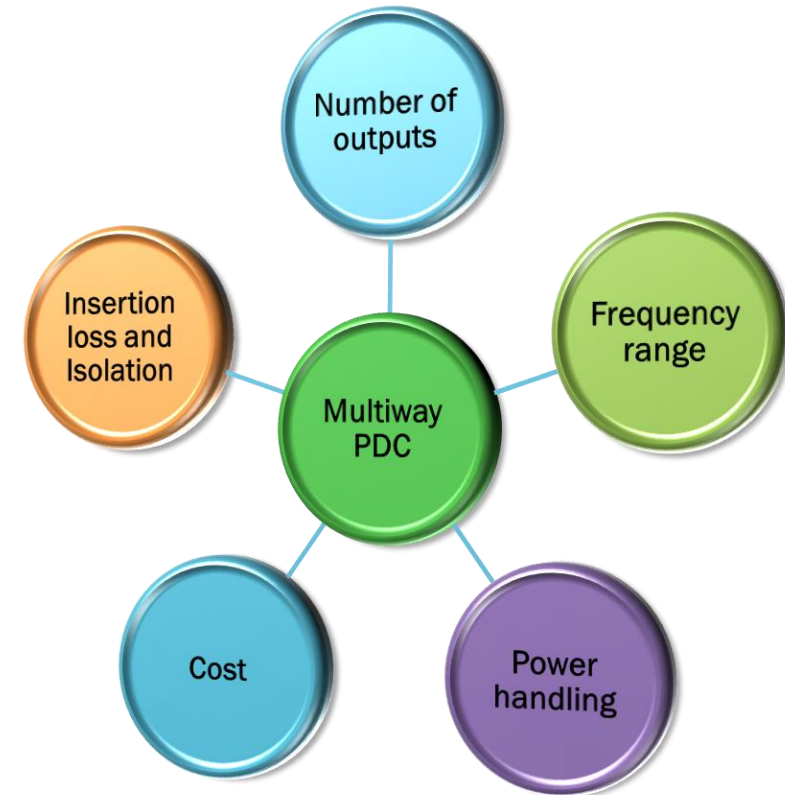
¹National Institute of Scientific Research (INRS),
University of Quebec, Montreal, QC, Canada

- Introduction
- Multiway PDC Problematic and Challenges
- State of art with Fixed Characteristic Impedance
- Theoretical Analysis
- Design Guidelines
- Experimental Results
- Conclusion

The multiway power divider/ combiner typically consists of a network of transmission lines that are designed to divide or combine the input signal into equal or unequal parts

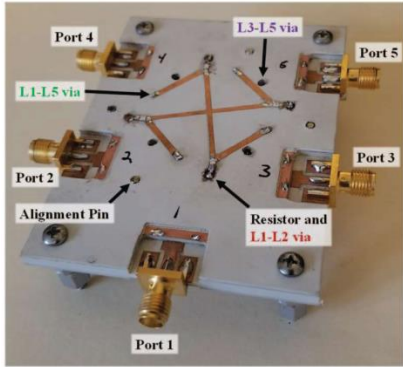


Multiway PDC Applications

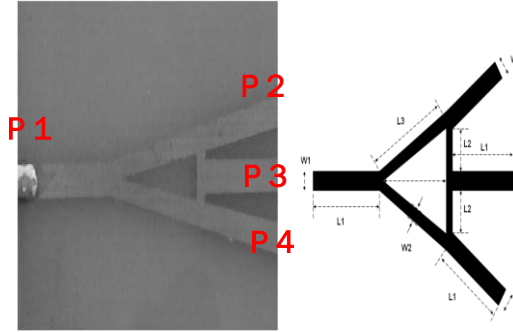
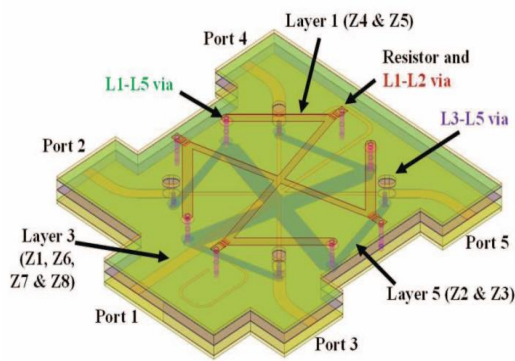


The performance of a multiway PDC

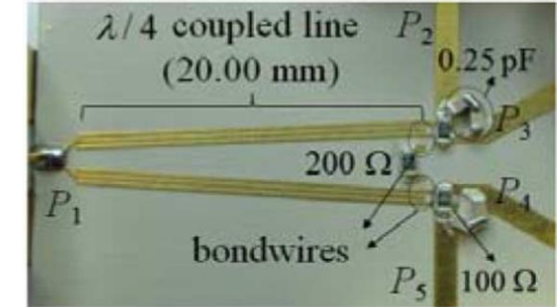
Multiway PDC Problematic and Challenges



4-Way PDC Based on MSL and stripline at 3 Ghz [1]



3-Way PD Based on MSL at 5Ghz [2]



4-Way PDC Based on MSL Coupled Lines at 2Ghz [3]

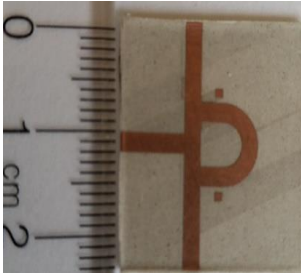
- The use of different TL widths in a design can add significant constraints on substrate selection and the fabrication process
- At higher frequencies, radiation loss and lumped element lengths must be carefully analyzed and considered.

[1] J. Furgal, K. Xu, J. H. Choi and J. K. Lee, "Broadband Equal-Split Planar 4-Way Power Divider/Combiner Suitable for High Power Applications," 2020 50th EuMC, Utrecht, Netherlands, 2021, pp. 840-843

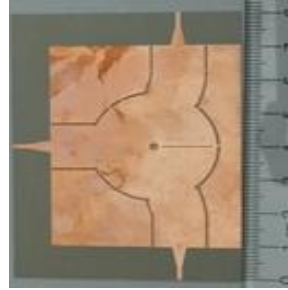
[2] G. -Y. Chen, J. -S. Sun, S. -Y. Huang and YD_Chen, "The Novel 3-Way Power Dividers/Combiners Structure and Design," 2006 IEEE AWMTC, Clearwater Beach, FL, USA, 2006, pp. 1-4

[3] S. Kim, S. Jeon and J. Jeong, "Compact Two-Way and Four-Way Power Dividers Using Multi-Conductor Coupled Lines," in IEEE Microwave and Wireless Components Letters, vol. 21, no. 3, pp. 130-132, March 2011

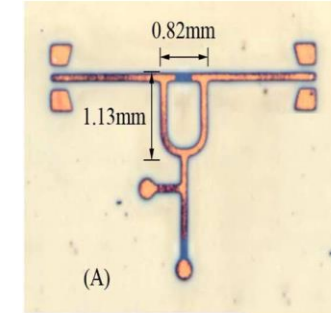
State of art with Fixed Characteristic Impedance



Gysel Power Divider
based on Microstrip
at 10 GHz [1]



Wilkinson Power based
Substrate-Integrated Waveguide
(SIW) at 10 GHz



Horst Power Divider
based on Microstrip
at 60 GHz

Benefits of using a fixed-width TL :

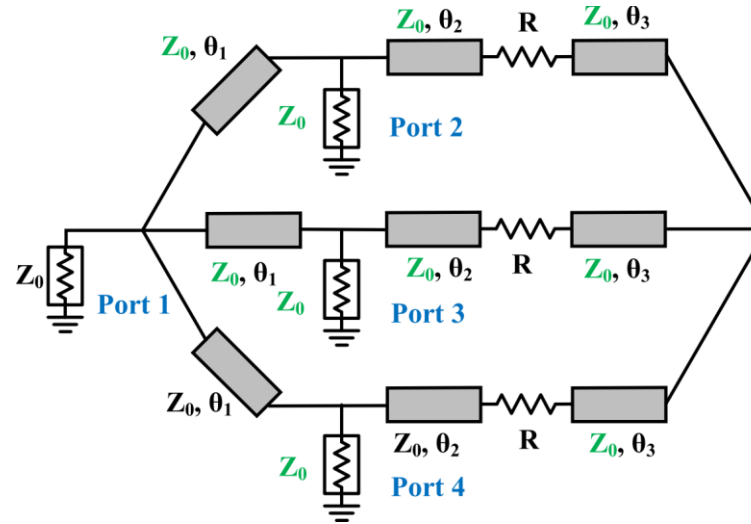
1. Help to minimize signal losses due to impedance mismatches
2. Allow great design flexibility in millimeter-wave circuits.
3. Help mitigate the effects of discontinuities, which can contribute to a reduction in radiation.

[1] A. Moulay and T. Djerfai, "Gysel Power Divider with Fixed Characteristic Impedance," 2020 IEEE/MTT-S IMS, Los Angeles, CA, USA, 2020, pp. 896-899

[2] A. Moulay and T. Djerfai, "Wilkinson Power Divider With Fixed Width Substrate-Integrated Waveguide Line and a Distributed Isolation Resistance," in IEEE MWCL, vol. 28, no. 2, pp. 114-116, Feb. 2018

[3] S. Horst, R. Bairavasubramanian, M. M. Tentzeris and J. Papapolymerou, "Modified Wilkinson Power Dividers for Millimeter-Wave Integrated Circuits," in IEEE TMTT, vol. 55, no. 11, pp. 2439-2446, Nov. 2007,

The proposed Two-Layer Three-Way PDC



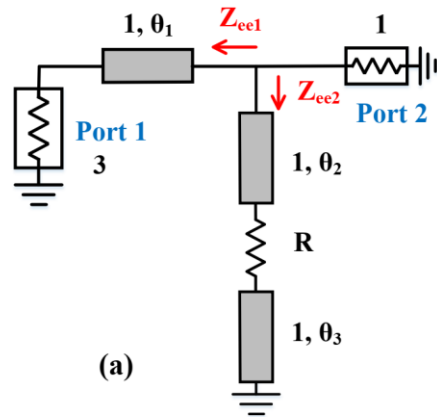
Proposed topology of the three-way PDC

- All sections have the same characteristic impedance Z
- A two-layer configuration enhances the isolation between opposite ports while maintaining compactness.

Even-even and odd-odd mode analysis

- Even-odd cases are similar to odd-odd cases, so only even-even and odd-odd cases were examined

Even-even

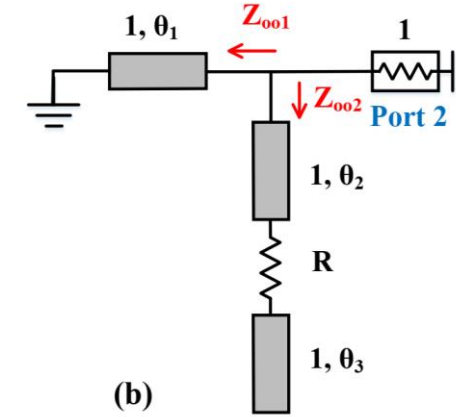


$$Y_{1ee} = (Z_{1ee})^{-1} = \left(\frac{3 + j \tan \theta_1}{1 + j 3 \tan \theta_1} \right)^{-1}$$

$$Y_{2ee} = (Z_{2ee})^{-1} = \left(\frac{\left(\frac{r}{z_0} - j \cot \theta_3 \right) + j \tan \theta_2}{1 + j \left(\frac{r}{z_0} - j \cot \theta_3 \right) \tan \theta_2} \right)^{-1}$$

$$= \left(\frac{\frac{r}{z_0} + j(\tan \theta_2 - \cot \theta_3)}{1 + \tan \theta_2 \cot \theta_3 + j \frac{r}{z_0} \tan \theta_2} \right)^{-1}$$

odd-odd



$$Y_{1oo} = (Z_{1oo})^{-1} = (j \tan \theta_1)^{-1}$$

$$Y_{2oo} = (Z_{2oo})^{-1} = \left(\frac{\left(\frac{r}{z_0} + j \tan \theta_3 \right) + j \tan \theta_2}{1 + j \left(\frac{r}{z_0} + j \tan \theta_3 \right) \tan \theta_2} \right)^{-1}$$

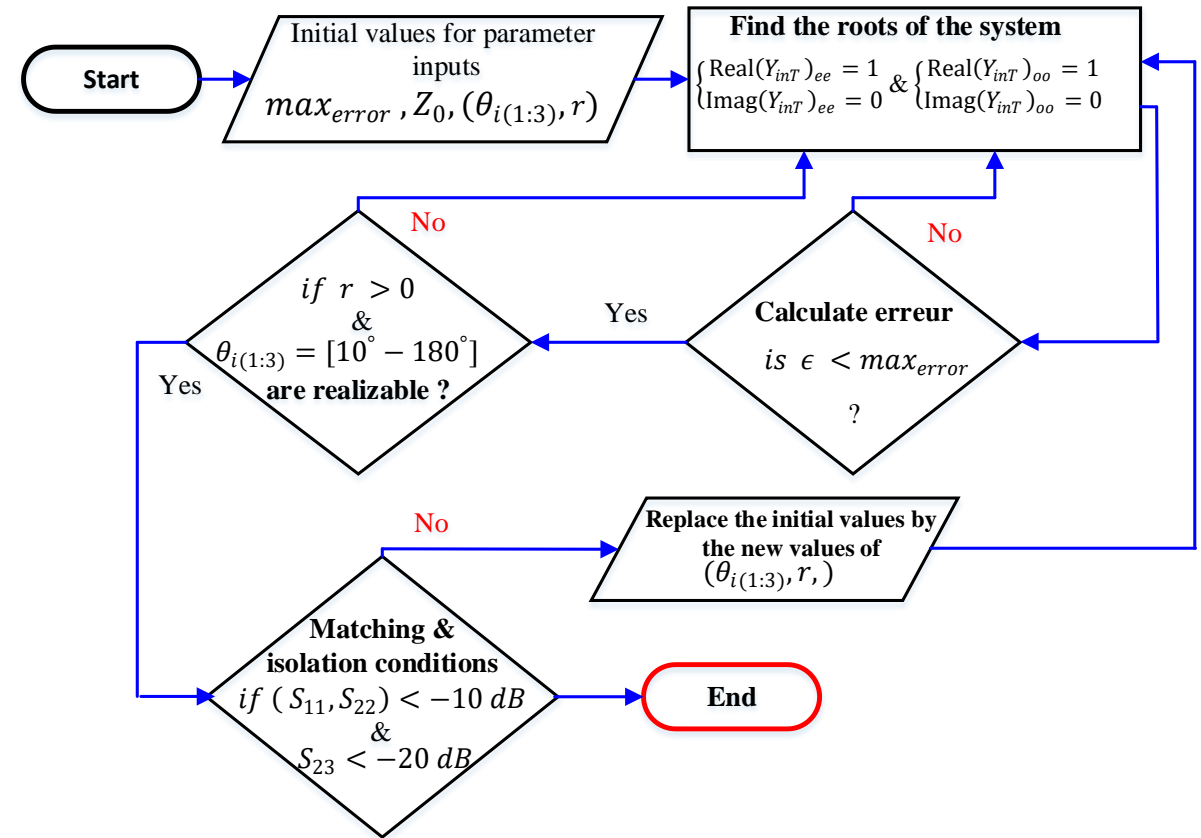
$$= \left(\frac{\frac{r}{z_0} + j(\tan \theta_2 + \tan \theta_3)}{1 - \tan \theta_2 \tan \theta_3 + j \frac{r}{z_0} \tan \theta_2} \right)^{-1}$$

Calculating PDC Parameters

The equality of the real and imaginary parts :

$$(Y_{1i} + Y_{2i})_{(i=ee,oo)} = 1$$

- Constant impedance Z reduces the unknown parameters of the circuit from 7 to 4 ($\theta_1, \theta_2, \theta_3, r$)
- The roots of the system of equations is found iteratively by using root-finding methods.
- Verify that the resistor values are real and positive and TL lengths are between $[10^\circ - 180^\circ]$
- Verify that both the matching and isolation conditions are simultaneously satisfied



Flowchart for calculating PDC parameters

Theoretical Bandwidth Calculation

- Input reflection coefficient

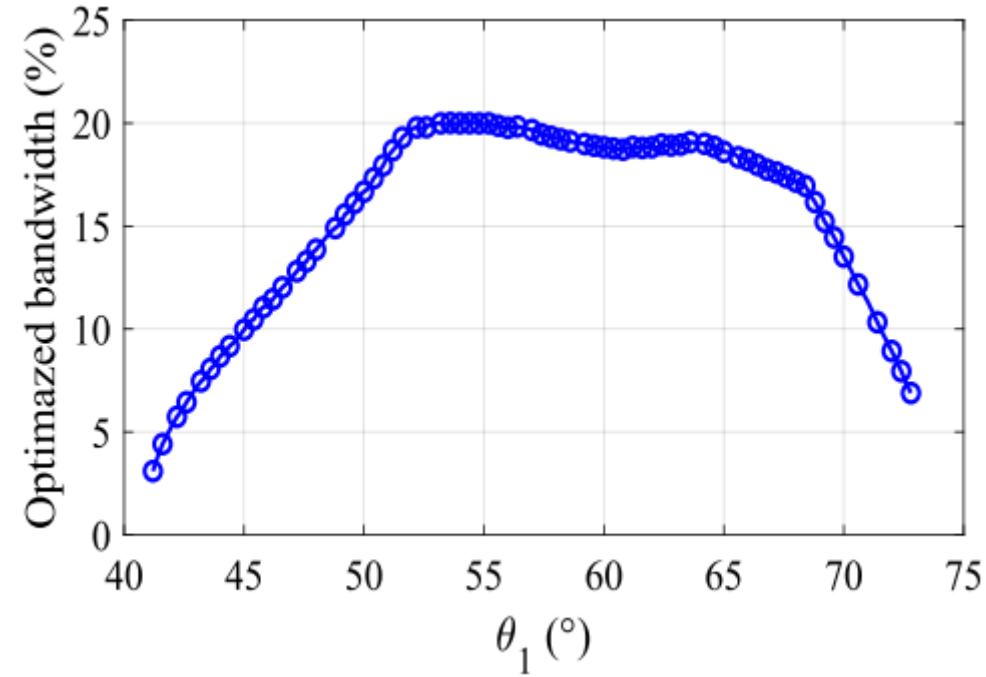
$$S_{11} = 20\log|\Gamma_{e,e}| \leq -10 \text{ dB}$$

- Output Reflection coefficient

$$S_{ii(i=2,3,4)} = 20\log\left|\frac{\Gamma_{e,e} + 2\Gamma_{o,o}}{3}\right| \leq -10 \text{ dB}$$

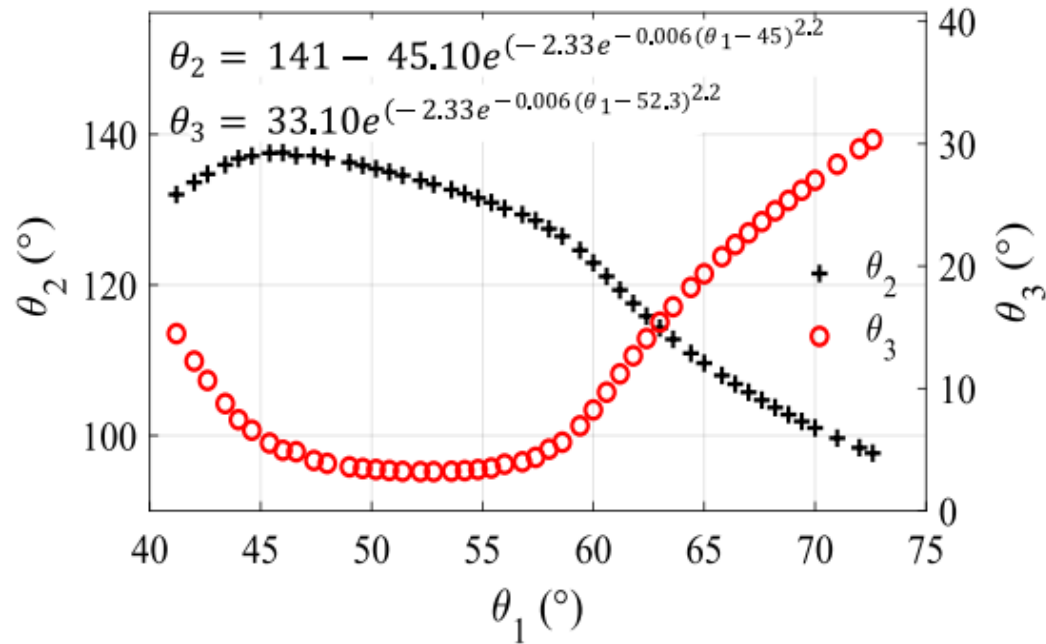
- Isolation coefficient

$$S_{ij(i=2,3,4; i \neq j)} = 20\log\left|\frac{\Gamma_{e,e} - 2\Gamma_{o,o}}{3}\right| \leq -20 \text{ dB}$$

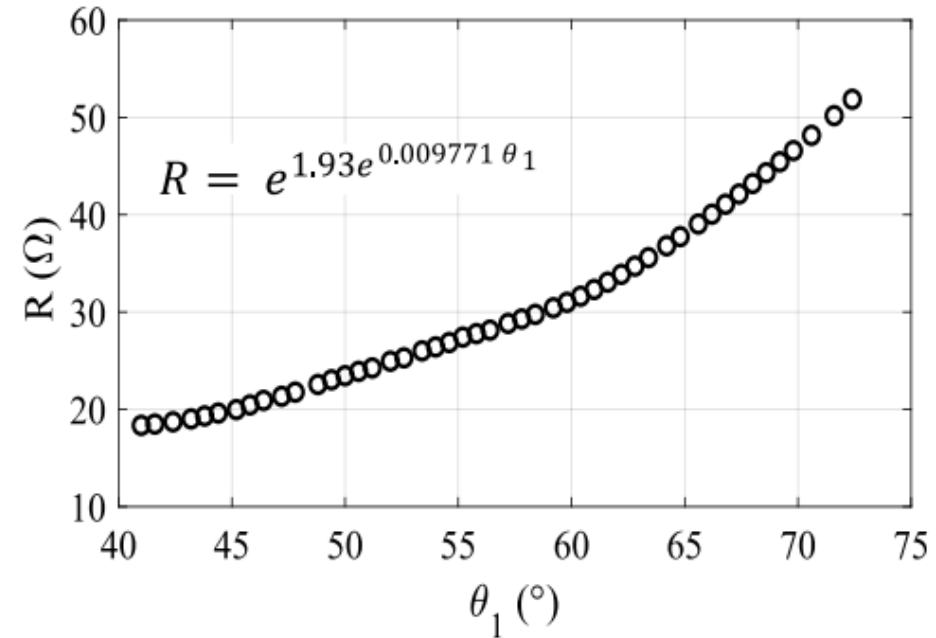


Bandwidth versus θ_1

Graphical representations with closed-form equations



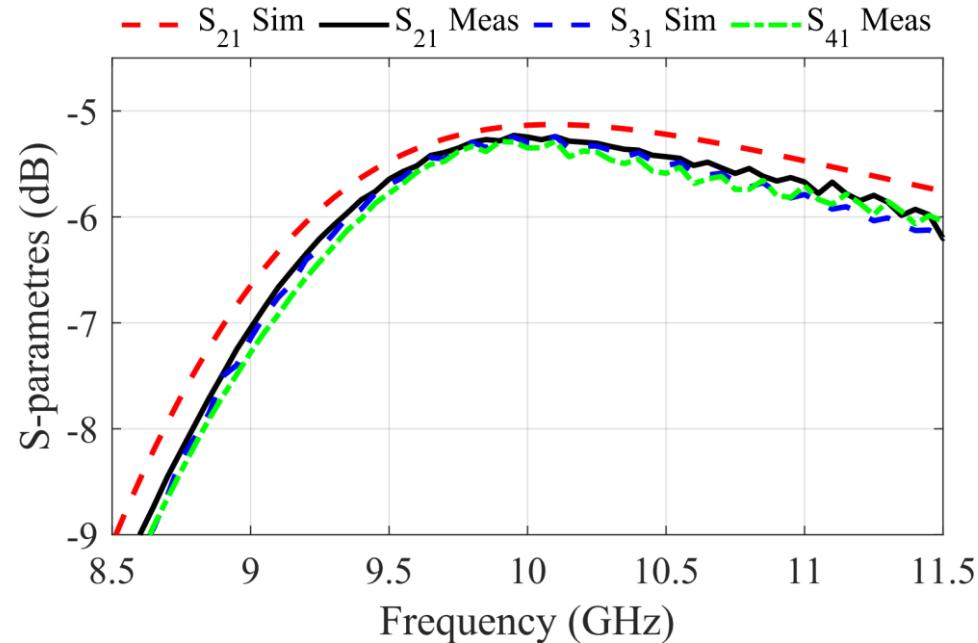
θ_2 and θ_3 versus θ_1



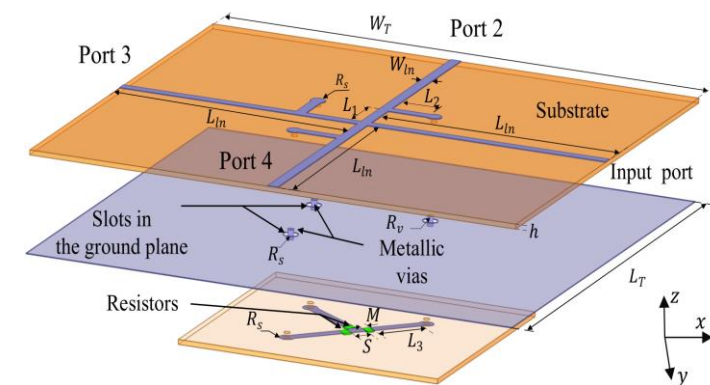
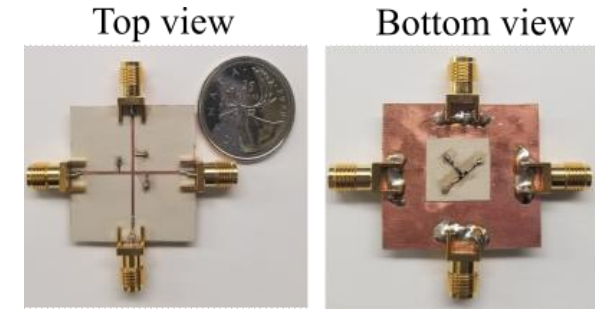
Resistance R versus θ_1

- The Graphical representations showed a slight discrepancy of 2% from the close-form equations.

Experimental Results



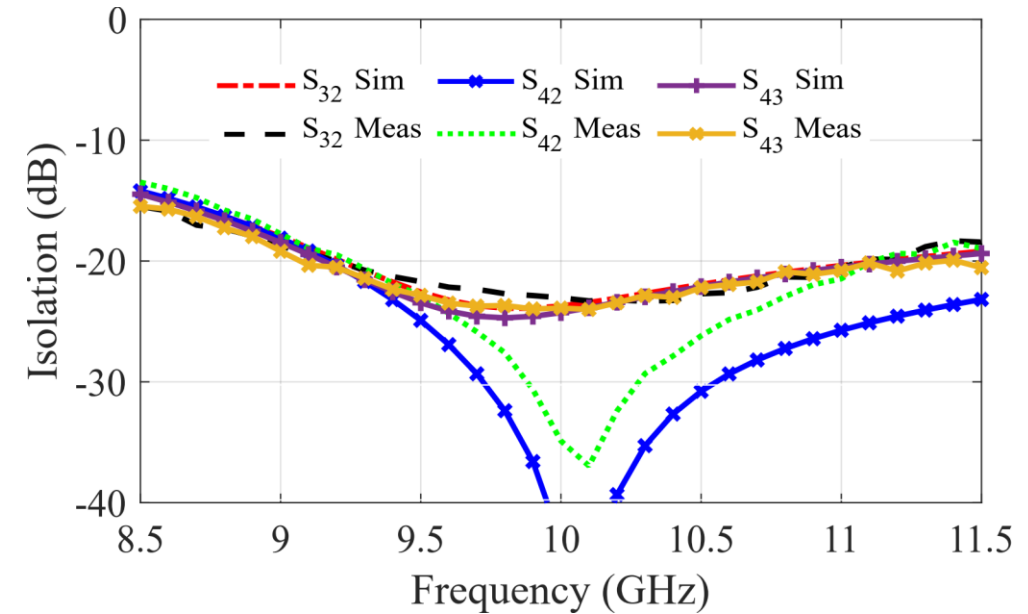
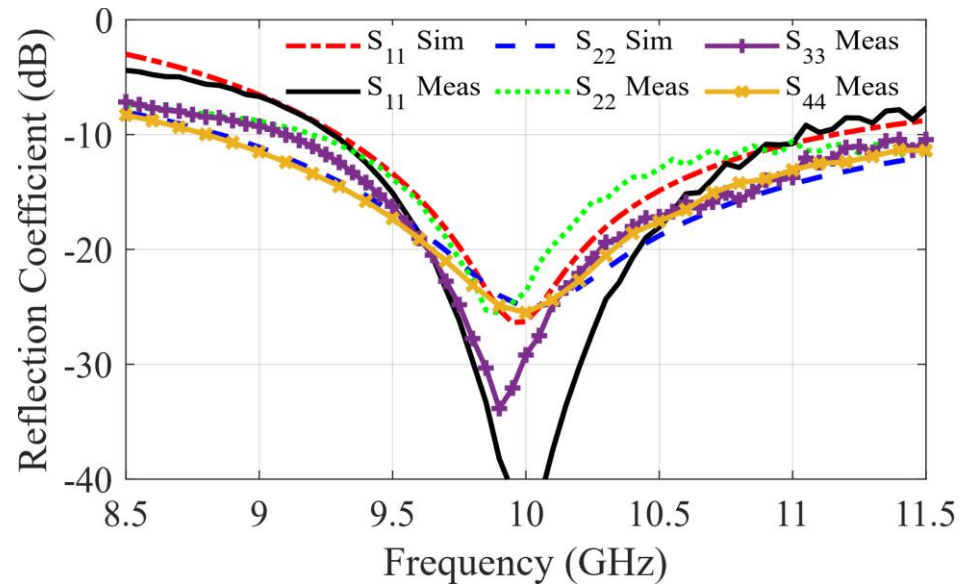
Fabricated Prototype



The 3-D view

- The transmission coefficient is between -5.2 and -6 dB over 2.3 GHz of bandwidth.
- The total length of the three arms is 190 deg which is smaller than 270 deg of the standard HPD and equivalent to the WPD.

Experimental Results



- Good matching better than 10 dB from 8.7 to 11 GHz
- The measured isolation between all the ports is higher than 20 dB over the 9.2-11.1 GHz

Conclusion

- ❖ Two-layer three-way power divider and combiner based on microstrip lines with fixed characteristic impedance was presented
- ❖ The design guidelines provide high flexibility, making the design process more accessible.
- ❖ Experimental prototypes demonstrate good matching and isolation performance over a broad fractional bandwidth, making it suitable for millimeter-wave applications
- ❖ This research opens up PDC design possibilities in any impedance characteristic with flexible bandwidth tailored to the specific needs of the application
- ❖ The proposed PDC design offers a simple, compact structure suitable for millimeter-wave applications that require a broader bandwidth.