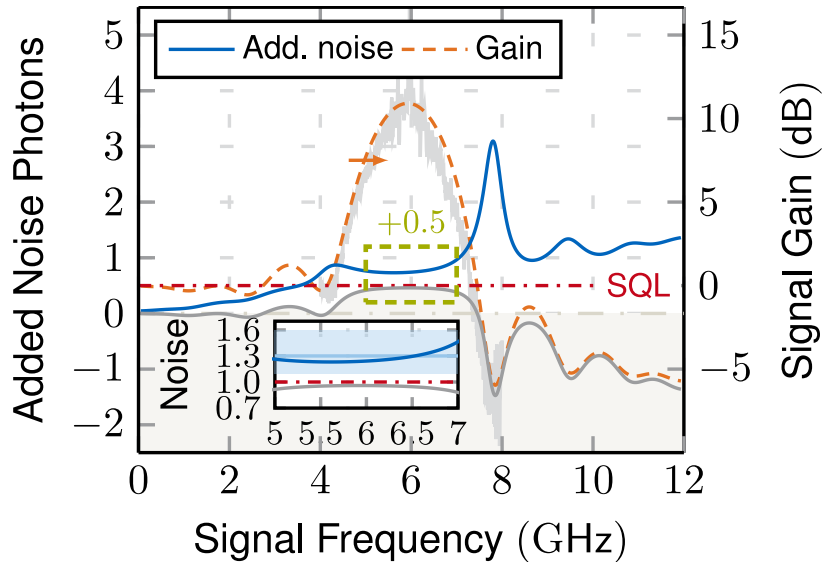


We4A-3

Quantum Models for Flux-Driven Superconducting Traveling-Wave Parametric Amplifiers with Different Nonlinear Junction Topologies

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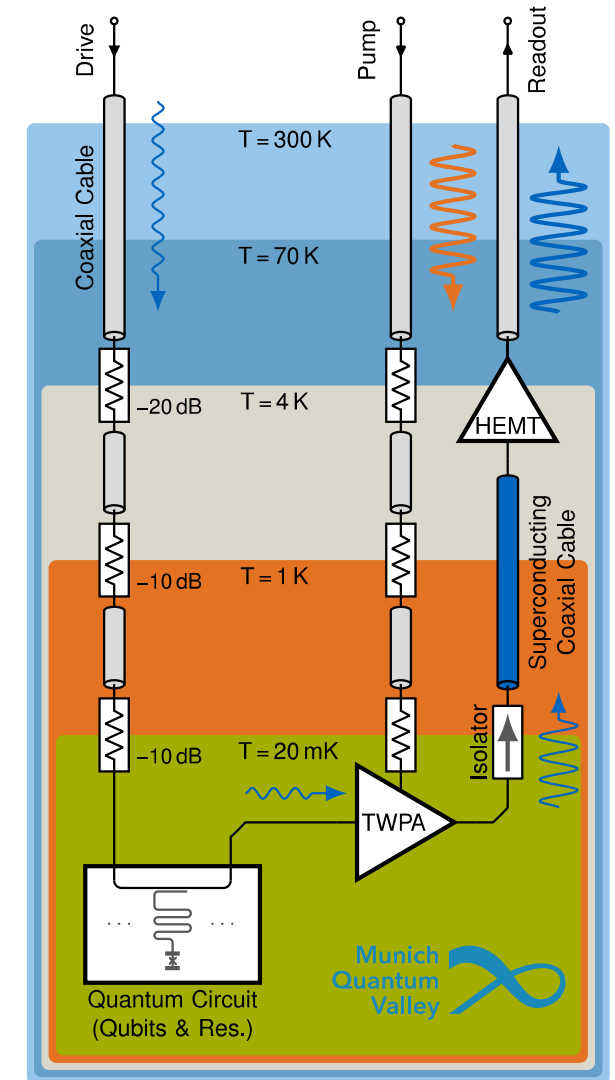
Technical University of Munich, Germany



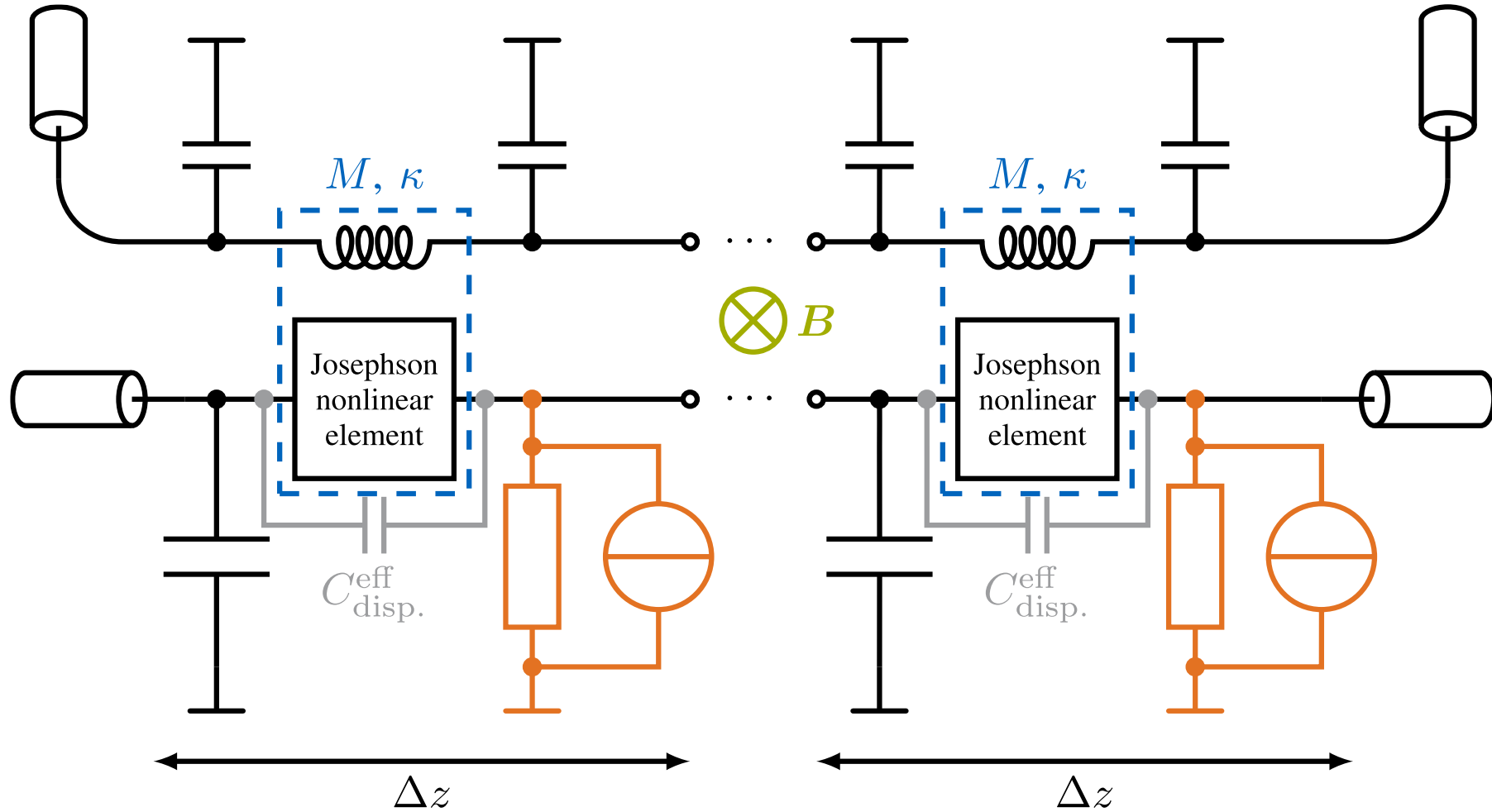
Yuan *et al.*, Phys. Rev. A **107** 022612 (2023)

Problem

- How to probe a qubit?
- Dispersive readout schemes
- Ultra-low-power signals
- High readout fidelity requires good SNR!
- Added noise needs to be close to the quantum limit!



Flux-Driven TWPAs – Circuit Model



- Taylor expansion of the current around a flux point φ^* with $i(\varphi^*) = 0$

$$i(\varphi) = i'(\varphi^*, \varphi_{\text{ext}}) \cdot (\varphi - \varphi^*) + \mathcal{O}(\varphi^2).$$

- Parametric amplification is achieved by a time-varying modulation of the **linear inductance**
- The effective potential with the effective flux operator

$$\hat{\varphi}_{\text{eff}} = \hat{\varphi} - \varphi^*$$

is given by

$$U_{\text{eff}} = \varphi_0 \int_{\varphi^*}^{\varphi} i(\varphi') d\varphi' = \frac{\varphi_0}{2} i'(\varphi^*, \varphi_{\text{ext}}) \cdot \varphi_{\text{eff}}^2.$$

Taylor expansion around Bias Flux

$$\begin{aligned} \hat{U} = & \frac{\varphi_0}{2} i'(\varphi^*, \varphi_{\text{ext}}) \Big|_{\varphi_{\text{ext}} = \varphi_B} \hat{\varphi}_{\text{eff}}^2 \\ & + \frac{\varphi_0}{2} \frac{di'(\varphi^*, \varphi_{\text{ext}})}{d\varphi_{\text{ext}}} \Big|_{\varphi_{\text{ext}} = \varphi_B} \underbrace{(\varphi_{\text{ext}} - \varphi_B)}_{\varphi_{\text{ac}}} \hat{\varphi}_{\text{eff}}^2 \\ & + \frac{\varphi_0}{4} \frac{d^2 i'(\varphi^*, \varphi_{\text{ext}})}{d\varphi_{\text{ext}}^2} \Big|_{\varphi_{\text{ext}} = \varphi_B} \underbrace{(\varphi_{\text{ext}} - \varphi_B)^2}_{\varphi_{\text{ac}}^2} \hat{\varphi}_{\text{eff}}^2. \end{aligned}$$

Nonlinear Coefficients

- By factoring out the critical current I_c , we can identify the nonlinear coefficients

$$c_2 = \frac{1}{I_c} i'(\varphi^*, \varphi_{\text{ext}}) \Big|_{\varphi_{\text{ext}} = \varphi_B}, \quad \leftarrow \text{Linear inductance}$$

$$c_3 = \frac{1}{2I_c} \frac{di'(\varphi^*, \varphi_{\text{ext}})}{d\varphi_{\text{ext}}} \Big|_{\varphi_{\text{ext}} = \varphi_B}, \quad \leftarrow \text{Three-wave mixing}$$

$$c_4 = \frac{1}{4I_c} \frac{d^2 i'(\varphi^*, \varphi_{\text{ext}})}{d\varphi_{\text{ext}}^2} \Big|_{\varphi_{\text{ext}} = \varphi_B}. \quad \leftarrow \text{Cross-phase modulation}$$

- The phase operator can be expressed in terms of creation and annihilation operators

$$\hat{\varphi} = \frac{\Delta z}{\sqrt{2\pi}} \int_0^\infty \frac{k(\omega)}{\varphi_0 \omega} \sqrt{\frac{\hbar k(\omega)}{2C'}} \hat{a}_\omega e^{ik(\omega)z - i\omega t} d\omega + \text{H.c.}$$

- Resulting Three-wave mixing Hamiltonian

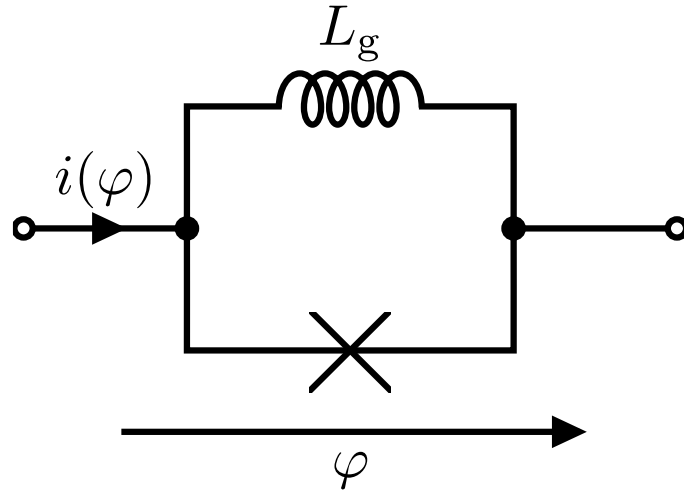
$$\begin{aligned} \hat{H}_{\text{WM}} = & - \int_0^x \int_0^\infty \int_0^\infty d\omega d\omega' dz \frac{i\hbar\kappa\omega_p C' f_\Lambda}{16\pi I_c} \cdot \frac{c_3}{c_2^2} \times \\ & \times \left[A_{p,0} \hat{a}_\omega^\dagger \hat{a}_{\omega'}^\dagger e^{i[k_p - k(\omega) - k(\omega')]z - i(\omega_p - \omega - \omega')t} + \text{H.c.} \right] \\ & + \int_0^x \int_0^\infty \int_0^\infty d\omega d\omega' dz \frac{\hbar\kappa^2\omega_p^2 \sqrt{\Delta z C'^3} f_\Lambda}{32\pi \sqrt{2I_c^3 \varphi_0}} \cdot \frac{c_4}{c_2^{5/2}} \times \\ & \times \left[|A_{p,0}|^2 \hat{a}_\omega^\dagger \hat{a}_{\omega'} e^{-i[k(\omega) - k(\omega')]z + i(\omega - \omega')t} + \text{H.c.} \right] \end{aligned}$$

Three-wave mixing

Cross-phase modulation

- Dispersion factor from Yuan *et al.*, Phys. Rev. A **107** 022612 (2023)

$$f_\Lambda = \sqrt{\omega\omega' \Lambda(\omega)\Lambda(\omega')} [\Lambda(\omega)\Lambda(\omega')]^{\frac{1}{4}}$$



- Induced flux

$$\varphi_{J,0} + \beta_L \sin \varphi_{J,0} = \varphi_{\text{ext}}$$

- Linear Inductance

$$i(\varphi) = I_c \left[\frac{1}{\beta_L} + \cos(\varphi_{J,0}) \right] (\varphi - \varphi^*) + \mathcal{O}(\varphi^2)$$

- Current-phase relation

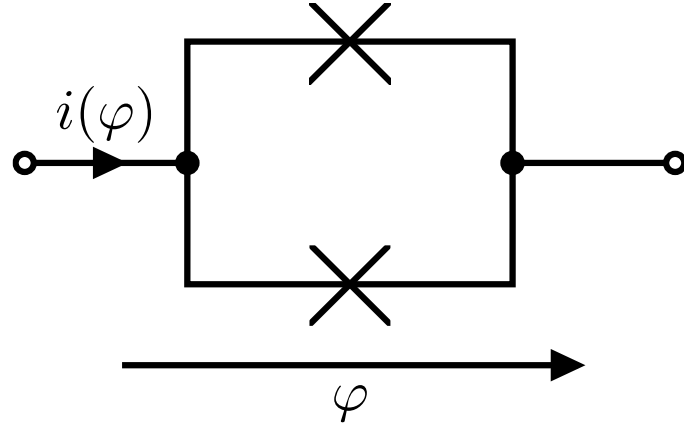
$$i(\varphi) = \frac{I_c}{\beta_L} \varphi + I_c [\sin(\varphi_{J,0} + \varphi) - \sin(\varphi_{J,0})]$$

Nonlinear Coefficients

$$c_2 = \frac{1}{2} \left[\frac{1}{\beta_L} + \cos(\varphi_{J,0}(\varphi_{\text{ext}})) \right] \Big|_{\varphi_{\text{ext}}=\varphi_B},$$

$$c_3 = \frac{1}{2} \frac{d}{d\varphi_{\text{ext}}} \cos(\varphi_{J,0}(\varphi_{\text{ext}})) \Big|_{\varphi_{\text{ext}}=\varphi_B},$$

$$c_4 = \frac{1}{4} \frac{d^2}{d\varphi_{\text{ext}}^2} \cos(\varphi_{J,0}(\varphi_{\text{ext}})) \Big|_{\varphi_{\text{ext}}=\varphi_B},$$



- Linear Inductance

$$i(\varphi) = 2I_c \left| \cos\left(\frac{\varphi_{\text{ext}}}{2}\right) \right| (\varphi - \varphi^*) + \mathcal{O}(\varphi^2)$$

- Current-phase relation

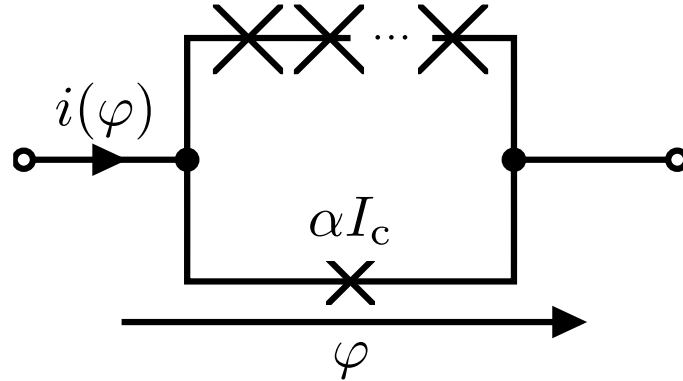
$$i(\varphi) = 2I_c \left| \cos\left(\frac{\varphi_{\text{ext}}}{2}\right) \right| \sin(\varphi)$$

Nonlinear Coefficients

$$c_2 = \left| \cos\left(\frac{\varphi_{\text{ext}}}{2}\right) \right| \Big|_{\varphi_{\text{ext}}=\varphi_B},$$

$$c_3 = \frac{d}{d\varphi_{\text{ext}}} \left| \cos\left(\frac{\varphi_{\text{ext}}}{2}\right) \right| \Big|_{\varphi_{\text{ext}}=\varphi_B},$$

$$c_4 = \frac{1}{2} \frac{d^2}{d\varphi_{\text{ext}}^2} \left| \cos\left(\frac{\varphi_{\text{ext}}}{2}\right) \right| \Big|_{\varphi_{\text{ext}}=\varphi_B}.$$



- Current-phase relation

$$i(\varphi) = \alpha I_c \sin(\varphi) + I_c \sin\left(\frac{\varphi - \varphi_{\text{ext}}}{n}\right)$$

- Asymmetry ratio $\alpha = 0.29$
- Number of large junctions $n = 3$

- Linear Inductance

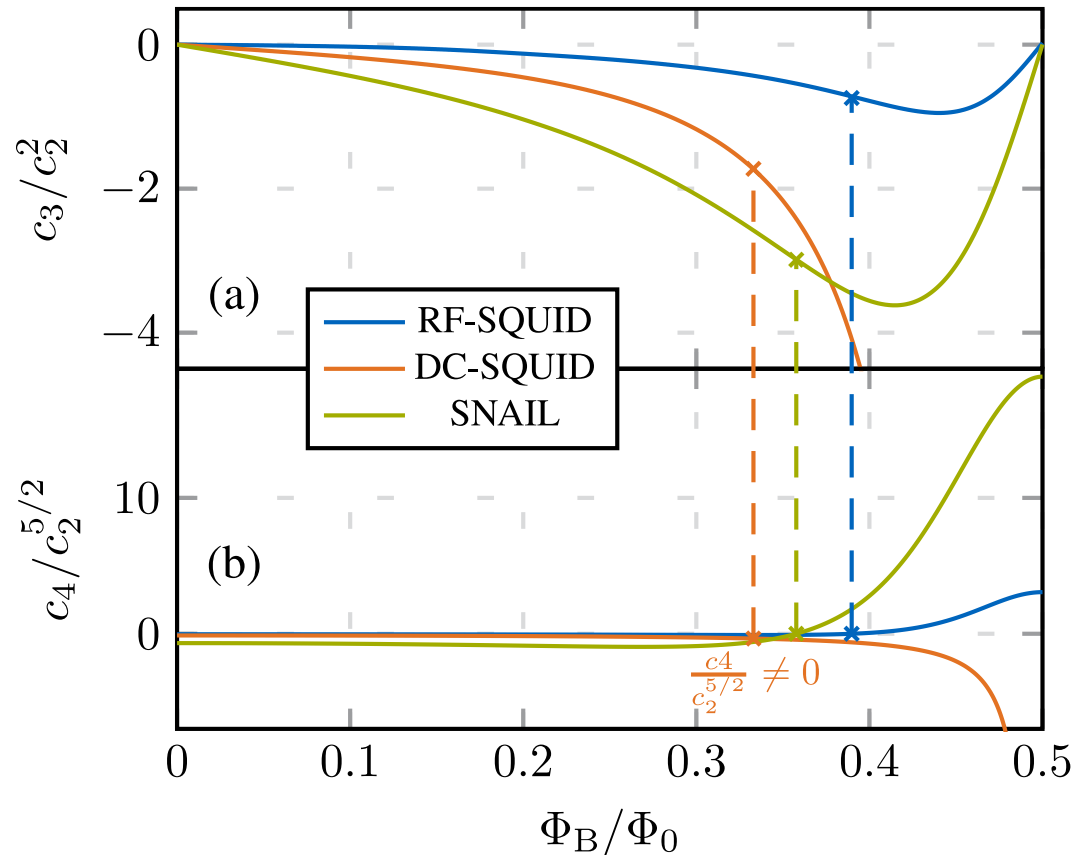
$$i(\varphi) \approx I_c \left[\alpha \cos(\varphi^*) + \frac{1}{n} \cos\left(\frac{\varphi^* - \varphi_{\text{ext}}}{n}\right) \right] (\varphi - \varphi^*)$$

Nonlinear Coefficients

$$c_2 = \frac{1}{2} \left[\alpha \cos(\varphi^*) + \frac{1}{n} \cos\left(\frac{\varphi^* - \varphi_{\text{ext}}}{n}\right) \right] \Big|_{\varphi_{\text{ext}} = \varphi_B},$$

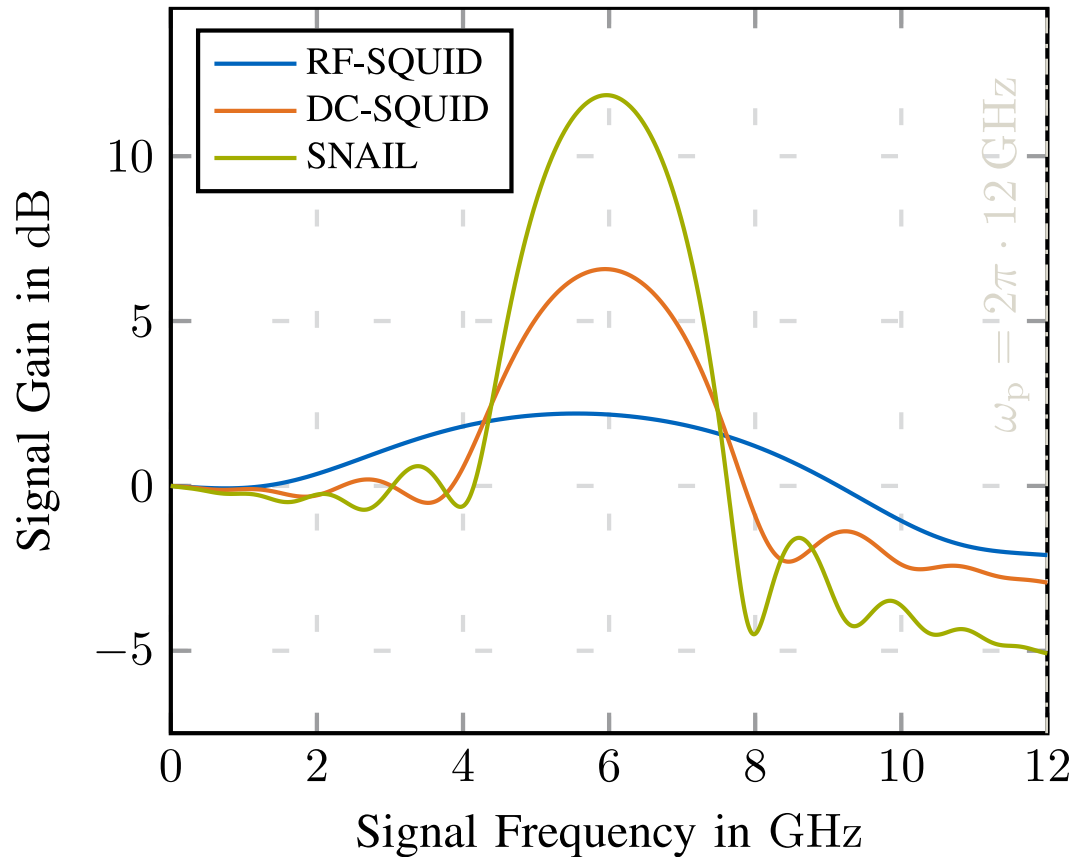
$$c_3 = \frac{1}{2} \frac{d}{d\varphi_{\text{ext}}} \left[\alpha \cos(\varphi^*) + \frac{1}{n} \cos\left(\frac{\varphi^* - \varphi_{\text{ext}}}{n}\right) \right] \Big|_{\varphi_{\text{ext}} = \varphi_B},$$

$$c_4 = \frac{1}{4} \frac{d^2}{d\varphi_{\text{ext}}^2} \left[\alpha \cos(\varphi^*) + \frac{1}{n} \cos\left(\frac{\varphi^* - \varphi_{\text{ext}}}{n}\right) \right] \Big|_{\varphi_{\text{ext}} = \varphi_B}.$$



- Largest 3WM coefficient for flux-driven SNAIL-based TWPAs
- No zero-XPM point for DC-SQUIDs
- Sign change at zero-XPM point for RF-SQUIDs and SNAILS which makes it possible to compensate for dispersion-induced phase mismatches

Results – 3WM Gain



- Largest 3WM gain (>10 dB) for flux-driven SNAIL-based TWPA
- Losses have been considered by a substrate with $\tan \delta = 0.0025$
- **Advantage:** Better separation between signal and pump modes

Conclusion

- General method for quantum mechanical Hamiltonians and equations of motion for flux driven traveling-wave parametric amplifiers
- Different junction topologies have been studied, where Superconducting Nonlinear Asymmetric Inductive Elements turned out to be favorable...

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